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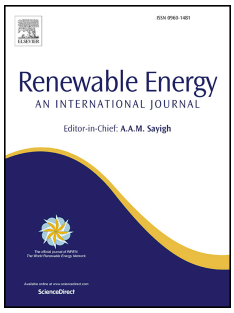

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Title: A standardised tidal-stream power curve, optimised for the global resource

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Abstract

Tidal-stream energy can be predicted deterministically, provided tidal harmonics and turbine-device characteristics are known. Many turbine designs exist, all having different characteristics (e.g. rated speed), which creates uncertainty in resource assessment or renewable energy system-design decision-making. A standardised normalised tidal-stream power-density curve was parameterised with data from 14 operational horizontal-axis turbines (e.g. mean cut-in speed was ~30% of rated speed). Applying FES2014 global tidal data (1/16° gridded resolution) up to 25 km from the coast, allowed optimal turbine rated speed assessment. Maximum yield was found for turbine rated speed ~97% of maximum current speed (maxU) using the 4 largest tidal constituents (M2, S2, K1 and O1) and ~87% maxU for a "high yield" scenario (highest Capacity Factor in top 5% of yield cases); with little spatial variability found for either. Optimisation for firm power (highest Capacity Factor with power gaps less than 2 hours), which is important for problematic or expensive energy-storage cases (e.g. off-grid), turbine rated speed of ~56% maxU was found – but with spatial variability due to tidal form and maximum current speed. We find optimisation and convergent design is possible, and our standardised power curve should help future research in resource and environmental impact assessment.

Keywords: tidal-stream energy; power curve; resource; optimization; renewable energy

1. Introduction

Tidal energy can be extracted using hydrokinetic devices or "in-stream" tidal-stream energy converters (e.g. Tsai and Chen, 2014; Masters et al., 2015), based on the principle that power (*P*) is a function of the cube of the volumetrically averaged current velocity (*u*) over the rotor swept area (*A*), turbine power coefficient (*Cp*) and seawater density (ρ):

$P = \frac{1}{2}\,\rho\, Cp\, A\, u^3$ [1].

As nations look to increase their renewable energy capacity in response to climate change (Neill et al., 2016) or improve access to affordable electricity (Goward-Brown, et al., 2019; Zhang et al., 2019), tidal-stream energy could offer one substantial renewable resource due to the predictability and reported power quality (Lewis et al., 2019). Three main types of tidal-stream turbines are in various stages of development (for a review, see Rourke et al., 2010): (1) horizontal axis turbines; (2) vertical axis turbines; and (3) rotating and reciprocating devices. This paper shall focus on the horizontal axis turbine, used for the majority of test and operational deployments; hence much data is available to inform and constrain our analysis – such as estimation of device efficiency and the device power coefficient (*Cp*: extracted power relative to the available power), alongside turbine behaviour parameters including turbine cut-in and rated speed (see Mason-Jones et al., 2012; 2013).

The potential of tidal-stream energy for a sustainable future is immense (~2.5TW M2 tidal energy is dissipated globally – see Egbert and Ray, 2001), with diverse applications: predictable contributions of renewable electricity to a national grid (Neill et al., 2016) to

energy solutions for remote communities and industries (e.g. Nielsen et al., 2018), such as contributing to UN sustainability goals and reducing energy poverty (e.g. Lozano and Taboada, 2020). However, the costs associated with tidal energy (e.g. Vazquez and Iglesias, 2015) such as cost reduction through economies of scale (e.g. Johnstone et al., 2013), and deployment constraints (e.g. Lewis et al., 2015), need to be reduced for the true potential of tidal energy to be realised. As power is proportional to the cube of tidal current, industry has predominately focused on turbines with high rated speed (>2.5m/s) at so-called "first generation sites (Lewis et al., 2015). It is unclear if mass-produced lower resource tidal-stream turbines for "high-value markets" could provide another route to cost reduction for the industry, and the motivation for this study.

As discussed in the US Dept. Energy "Powering the Blue Economy" (LiVecchi et al., 2019), there is a diverse range of potential power demands (e.g. both in size and timing of power required) and higher value markets (thus economic viability). We hypothesise that previous focus on MegaWatt-scale contributions from tidal-stream turbines (with high rated speeds above 2.5 m/s) is creating uncertainty and may not be suitable for all potential renewable energy markets (LiVecchi et al., 2019). For example, there has been a reported need for power curves to aid resource mapping studies with one (1 m/s cut-in and 2.7 m/s rated) predominately being applied tidal turbine design (e.g. Hardisty 2012; Vennel et al., 2015; Robins et al., 2015) which may introduce bias in resource assessment (Fairley et al., 2020). Furthermore, Robins et al. (2015) proposed that turbines suitable for lower flows would reduce temporal variability to the resource and increase resultant net power. Tidal-stream energy resource therefore appears uncertain, in part, due to uncertainty of end-user power needs and device design.

Mapping the tidal resource for a region relies on validated hydrodynamic models, which numerically solve versions of the Navier-Stokes equations to fully capture tidal dynamics. Theoretical resource estimates for a region calculate tidal power from the ocean model output variables to be applied in equation 1. Tidal resource has been shown to be affected by the power extracted (e.g. Garrett and Cummins, 2005; 2007; Yang et al., 2013), hence technical resource assessment often explicitly include power extraction of tidal turbines to further improve potential yield estimates (e.g. Vennell et al., 2010; Goward-Brown et al., 2017). Environmental impact assessments to the deployment of tidal turbines also require power extraction to be explicitly resolved in the ocean model simulations; for example, impacts to circulation and associated processes (e.g. Kadiri et al., 2012), sediment transport pathways (Robins et al., 2014) and morphodynamics (Neill et al., 2009).

The drag force (*Fd*) of a tidal turbine is represented within hydrodynamic model simulations applying equation 1 as:

$Fd = \frac{p}{u}$ [2];

hence the impact of tidal energy conversion can be explicitly resolved in environmental impact and resource assessments (see Yang et al., 2013). Tidal-stream turbine behaviour is predominately based on first generation technologies (Lewis et al., 2015); where cut-in speed (*Vs*), and rated speed (*Vr*: the current speed where maximum or "rated power" (*Pr*) is extracted, with power "capped" or "shed" for current speeds above *Vr*) – must be resolved to adequately represent turbine behaviour (e.g. Goward-Brown et al., 2017). First generation tidal-stream turbines are defined by Lewis et al. (2015) as having a rated speed ~2.5 m/s, and, whilst many devices indeed have high rated speeds, a number of lower flow devices (e.g. Kites – see Buckland et al., 2015) and applications (O'Donncha et al., 2017) have been discussed. Indeed, in many resource assessments, power curve information has been stated as necessary for future work (e.g. Lewis et al., 2015; Vazquez and Iglesias, 2015; Guillou et al., 2018).

The lack of data to parameterise turbine behaviour presents a significant challenge due to uncertainty in the parameterisation of tidal-stream turbine behaviour. The impact of various tidal turbine power curves to the technical resource assessment is shown in Figure 1; where a 15-day time-series of two harmonics (M2 amplitude of 2 m/s and S2 amplitude of 0.5 m/s) is applied to estimate theoretical power density (*P/A* using Eq. 1), and the theoretical power curve of two devices: *Vr*=2.5 m/s and *Vs*=1 m/s (from Lewis et al., 2015), and *Vr*=2 m/s and *Vs*=0.5 m/s (from Encarnacion et al., 2019). Although rated turbine speed (*Vr*) differs by 0.5m/s between the two devices of Figure 1, with mean power and mean daily energy difference of 18% and 23% respectively, the maximum drag (thus impact, estimated from Eq. 2) differed by 41%. Moreover, the Capacity Factor (*CF*), defined here as the ratio of energy converted relative to the maximum energy that could be converted (i.e. if at rated power throughout the time-series), varied by 14% between the two devices of Figure 1; with a 19% difference in the time of zero power (so called downtime) and a 2 hour difference in the longest duration window of zero power output, which has implications for storage design and whole system costs.

Given that tides are almost entirely deterministic (e.g. Lewis et al., 2019), and the wide variety of potential markets globally (from large-scale power contributions to national electricity distribution networks to remote “off-grid” industries and communities): are the present range of tidal-stream turbine designs suitable for all global markets, and can a scalable convergent solution be found? This paper aims to firstly consolidate the diverse range of horizontal axis tidal turbines to a scalable power curve for unbiased resource and impact assessments. The standardised power-density curve can then be applied to explore convergence based on the global tidal-stream resource. We do not include the swept area in our analysis as this is likely to be based on local bathymetric constraints, life cycle assessment and cost optimisation. Instead our objective is to establish a method, which can be applied in the future to include cost optimisation based on future markets and mass-production principles (Junginger et al., 2004; Johnstone et al., 2013): providing a constructive step towards a resource-led globally-optimal engineering solution for the renewable energy industry.

2. Method

This study is composed of three parts: firstly, power curve data is compiled for the majority of published horizontal tidal-stream turbines (i.e. all that could be found). Rated power (*Pr*) and flow speed (*Vr*) allow the power coefficient (*Cp*) and thrust coefficient (*Ct*) to be estimated, using variables from equations 1 and 2, because:

$Ct = \frac{2\,F}{\rho\,A\,u^2}$ [3];

$Cp = \frac{2\,P}{A\,\rho\,u^3}$ [4].

Consolidating the data, a normalised theoretical mean power density curve relative to rated power (i.e. *P/Pr* and *u/Vr*) can be established (i.e. swept area removed), and also compared to observed variability in a grid-connected tidal-stream turbine (published in Lewis et al., 2019). Here, density of seawater (ρ) is assumed to be 1027 kg/m^3 and the turbine is operated at constant Tip Speed Ratio (TSR) irrespective of swept area (*A*) or flow speed (*u*): i.e. that *Cp* does not vary with flow speed and Tip Speed Ratio (Mason-Jones et al., 2012; 2013).

The second part of our method will apply the average power density curve information (which we call the normalised power curve) to resolve optimal power curve characteristics for the diverse range of potential markets and tidal energy sites globally: for example, does the optimal power curve for a remote island/industry differ to an optimal tidal power curve for electricity supply to a grid?

Depth averaged tidal current information was based on the FES2014 dataset (Finite Element Solution data assimilated global tide model), which has a global grid resolution of 1/16° (Carrere et al.,, 2015). The FES2014 dataset was masked using the NASA distance-to-coast dataset (resolution 1/25°) which was created using the Generic Mapping Tools (GMT) coastline. Global tidal data of the four principal semi-diurnal and diurnal tidal constituents (M2, S2, K1, O1), between latitudes 70°S and 70°N and included only ocean grid cells that were within 25 km from land were extracted. We assume tidal energy development beyond 25 km is not economically feasible based on challenges with connecting to shore, and have removed tidal analysis from high latitude (>70°) due to ice interaction challenges and uncertainties.

Applying the normalised power curve to a wide range of rated speeds (*Vr* discretised in 0.1 m/s bins between 0.3 m/s and 6 m/s) allows power density curves for all potential tidal-stream turbines to be applied to one year tidal current time-series (5 min frequency). The tidal current time-series at each location was calculated using the "t_tide" toolbox: a harmonic tidal prediction method, where a time-series is described from the sum of sinusoids at frequencies specified from astronomical parameters (Pawlowicz et al., 2008). Global tidal harmonics data were used from the FES2014 product (Carrère et al., 2015; Lyard et al., 2020) for all resolved coastal locations (<25 km from land). An optimal power density curve was selected for each site using three scenarios (A, A2 and B) to represent the diversity of end user needs; from weighting the optimal tidal turbine power density curve based on firm and constant power, or maximum possible yield. Hence, the range between high yield and firm power (scenarios A and B) should therefore represent all potential optimal tidal turbine solutions; providing a sensitivity test to power curve choice in resource assessment, but also the potential for current technologies and concepts to be scaled for the more globally prevalent, lower flow and power demand markets.

Scenario A (maximum yield): the power density curve that gave the highest annual energy yield for each site (irrespective of storage and end user needs). We assume such a scenario useful in free-market economic systems with national electricity distribution networks.

Scenario A2 (high yield): the highest Capacity Factor (CF) for power density curves that gave the top 5% of annual yields per site. Therefore, although Scenario A2 does not bound the range of potential optimal tidal power curves, it is assumed to represent a likely choice given other resource uncertainties (e.g. higher order tidal harmonic effects, or the impact of waves (Lewis et al., 2014) and weather windows).

Scenario B (Firm yield): the highest yield power density curve that had a maximum gap in power generation below 2 hours and consistent peak power (within 2%). We assume such a firm power tidal turbine beneficial for users where likely storage potential is low, or the storage costs are high (for example the use of fly wheels instead of batteries).

The third part of method aims to resolve convergence in an optimal power curve based on the global tidal data; producing simplified rules for industry and researcher to follow (e.g. can we assume tidal turbine rated speed to be equivalent to the peak spring tidal current speed for a given site?) Finally, we investigate the impact of tidal data quality by comparing our 1/16° FES2014 results to that derived from tidal harmonics calculated using a much higher resolution ocean model at 1/100° (~1km instead of ~7km spatial resolution) for the UK domain (14°W to 11°E, and 42°N to 62°N). Data were interpolate onto the higher resolution grid and the data of the UK ROMS model details given in Robins et al. (2015).

3. Results

Horizontal-axis tidal-stream turbine power density curves were normalised and standardised (Section 3.1), which can be applied to idealised tidal current time-series with increasing

complexity in tidal harmonics (Section 3.2), and applied to the global tidal harmonic data in Section 3.3.

3.1. Power curve analysis results

Horizontal axis tidal turbine information was gathered from published data of 14 devices that are in commercial development or deployment (Table 1). We believe data in Table 1 to be the most comprehensive, up-to-date list compiled thus far. We acknowledge that Table 1 is incomplete, with some prototypes and models missing, however convergence of the normalised power-density curve in Figure 2 is clear – and the addition of devices likely to only impact parameters that are not considered here (e.g. swept diameter mean rated power). Where key variables are missing (noted in Table 1 with *), data were extrapolated using equations 1 and 4.

The rated power density and speed (*Pr* and *Vr* respectively) of the tidal-stream turbines are shown in Figure 2a, compared to the theoretical (black dash line). Normalised power-density curves of these devices are shown in Figure 2b, using the mean device power coefficient (*Cp*) of Table 1, assuming *Cp* constant through all flow speeds, alongside the measured power variability (at 0.5 Hz frequency) for a "grid connected" tidal-stream turbine (taken from Lewis et al., 2019). Measured fine-scale power fluctuations of Figure 2b, likely due to fine-slow flow variability and turbulence (see Lewis et al., 2019), were found to be much larger than variability in mean device characteristics (cut-in and rated speed) for the 14 devices. Therefore Figure 2 indicates a normalised mean power curve can be used to represent all horizontal axis tidal turbines currently being developed, and apply the power-density curve to global tide data in Section 3.2. Finally, Figure 2a shows there is no trend in diameter of the swept rotor area, especially considering the size range of turbines, shown by the large standard deviation in Table 1, hence further justification to use power density in our analysis - as rotor size is likely to depend on local site charactersitics and cost-benefit analysis (which is beyond the scope of this work).

A standardised and normalised power curve for horizontal axis tidal-stream turbines was established using the mean value of Table 1: Cut in speed of the turbine (*Vs*) was found to be 30% of the rated speed (*Vr*) on average with a standard deviation (STD) of 7%, and we assume power coefficient (*Cp*) is constant, at a mean value of 0.37; which allows the power density (*P/A*) to be described relative to the rated power of a device (where *Pr* is expressed as *P/A* relative to the rated, thus between 0% and 100%). It should be noted that the power coefficient (*Cp)* is likely to be affected by a number of variables: flow speed and site turbulence characteristics (including waves), as well as blade design and Tip-Speed-Ratio (see Mason-Jones 2012; 2013) – however the variability does not significantly affect our results (based on unpublished sensitivity test – varying section 3.2 with *Cp* with one STD: 0.04).

The standardised power curve, based on mean values of Table 1, is shown in Figure 3a and is described in equation 5, using three conditions:

$$\text{When } \mathrm{Vr} > \mathrm{u} > 0.3\mathrm{Vr}: \mathrm{P} = \frac{1}{2} 0.37\ \mathrm{u}^3 \mathrm{A}\,;$$

$$\text{when } \mathrm{u} < 0.3\mathrm{Vr}: \mathrm{P} = 0;$$

$$\text{when } \mathrm{u} > \mathrm{Vr}: \mathrm{P} = \mathrm{Pr} \quad [5].$$

Moreover, the normalised drag and thrust coefficient (*Ct*) can now also be described (using Equation 2) – which allows a tidal-stream turbine, unbiased in technology choice, to be represented for future resource and environmental impact assessment hydrodynamic modelling methods. The device agnostic power curve of Figure 3 therefore only needs a rated power (*Pr*) and swept area (*A*) to be assumed, and we shall explore an optimal *Vr*, based on tidal resource, in Section 3.2

3.2. Power density curve optimisation

The standardised normalised power curve of Figure 3 was applied to a tidal current time-series for a range of rated turbine speeds (*Vr*), with the Capacity Factor (*CF*) and the yield for each theoretical device compared. Capacity Factor (*CF*) was calculated as the percentage of energy captured compared to energy captured if a turbine was at rated speed throughout the timeseries:

$CF = \frac{\int \frac{1}{2} Cp\, A\, u_t^3}{\int \frac{1}{2} Cp\, A\, Vr^3}$ [6]).

Here, we consider power-density in our analysis, as bathymetry likely to be uncertain in the spatially coarse global data of FES2014 (1/16° see Section 3.3) and we assume swept area (*A* in Eq. 1) to be controlled by cost and array-design optimisation. Furthermore, the scaling of depth-averaged current (*u*) to hub-level flow is not included but cannot be represented in global tide data due to sub-scale temporal and spatial variability. The swept area (*A*) can be removed from our *CF* calculation (of Eq. 6), as it is a constant in the numerator and denominator integral; therefore our optimisation is independent of swept area, and instead our analysis focuses on the rated speed of a turbine relative to the temporal variability of the tide for a given site.

The mean power density and mean daily yield (kWh/m^2 per day) were also calculated as metrics of power curve performance for each theoretical power curve at each site. To demonstrate the method, Figure 4 shows the optimal power density curve (Figure 3, with rated turbine speeds between 0.3 m/s and 6.0 m/s in 0.1 m/s increments) for an idealised tidal current, with a single M2 (principal lunar semi-diurnal tidal harmonic) of amplitude 2 m/s (hence each peak current is 2 m/s with no variability between tides). The optimal power curve for the simplified case of Figure 4 is a turbine with a rated speed at 2 m/s (as expected), with an optimal mean power and yield density of ~0.6 kW/m^2 and 15 kW/m^2 per day respectively (corresponding *CF* of 41%).

Increasing the complexity of an idealised tide example, we demonstrate the power density optimisation for a site with two harmonics in Figure 5: M2 and S2 (principal solar semi-diurnal harmonic), which together simulate the fortnightly “spring-neap” cycle that describes 75% of UK tidal variability (Robins et al., 2015). Figure 5 demonstrates the optimal power curve for an extreme case, where the S2 amplitude is 60% of the M2 signal (M2 amplitude = 1 m/s), such that peak current of 1.6 m/s occurs when M2 (period 12.42 hours) and S2 (period 12 hours) are in-phase (spring tide), and 0.4 m/s peak current speeds occur when M2 and S2 are out-of-phase (neap tide). Optimal yield for Figure 5 was found when the turbine rated speed was that of the peak spring tide (*Vr*=1.6m/s) but with a much reduced Capacity Factor (17%), due to the extreme nature of the M2/S2 ratio. The importance of weighting the optimal tidal power curve to either yield (i.e. Scenario A or A2) or consistent power (i.e. Scenario B) is demonstrated in Figure 6.

Variability in choice of an “optimal” power curve, described here as rated turbine speed (Vr) relative to the M2 current amplitude (thus *Vr*/UM2), is demonstrated in Figure 6 for the range of M2/S2 ratios (M2/S2 of 0 has only an M2 tide, whilst equal M2 and S2 current amplitudes has a ratio of 1), with four metrics of turbine performance that were calculated applying the idealised power density curve of Figure 3 to a rated turbine speed between 0.3 m/s and 6 m/s (in steps of 0.1 m/s): hence Figure 6 is independent of resource magnitude. The four metrics of turbine performance in Figure 6 were based on yield performance relative to the maximum (Capacity Factor in Figure 6a and yield as a percentage of the maximum possible yield Figure 6c), and the persistence of power supply: percentage of time no power is produced in Figure 6b (as opposed to percentage of time at rated power of Figure 6a) and the largest “power gap” where no power is produced (Figure 6d). The choice of what an “optimal” tidal-stream turbine is clear at the extremes of the M2/S2 ratio in Figure 6, where, although extreme, a turbine with a relatively high rated speed

would produce large/largest yield but with a low CF and large gaps in power production (thus having consequences in the design and cost of storage and power distribution).

A large number of constituents are needed to describe the complex processes which give realistic tides (hour-to-hour and day-to-day variability in current speed); for example, the K1 and O1 constituents together describe the diurnal inequality (one tide bigger than another in a given day for semi-diurnal tidal systems), which, with the M2 and S2 constituents, can describe tidal form (F value) and thus the diurnal (one tide per day), semi-diurnal (two tides per day) or "mixed" nature of a tide at any site (Robins et al., 2015). The complexity of the power curve optimisation, based on resource, is further developed from Figure 6 by using these four principle constituents (see Figure 7). Figure 7 shows theoretical turbine performance for yield (panel a) and persistent power (panel b) for all possible turbine power-density curves (*Vr* 0.3-6 m/s) when varying an idealised tidal current based on the tidal dorm (F value), calculated as the relative magnitude of diurnal and semi-diurnal principle constituents (see Robins et al., 2015):

$$F\ value = \frac{K1+O1}{M2+S2} \quad [7].$$

Unlike Figure 6, the result of Figure 7 was found to be affected by the M2/S2 ratio as multiple combinations of four constituent amplitudes can produce the same F value: Therefore, the result of Figure 7 is based on a tide with a M2 amplitude of 1m/s and S2 amplitude being 0.1 m/s (M2/S2 = 0.1). Hence, it should be noted that the result of Figure 7 would be different if the F value was the same but the M2/S2 ratio were different (based on sensitivity test, an example of which is shown in Appendix Fig. A1). The tidal-stream power density curve optimisation algorithm, which selects the rated speed (*Vr*) for Scenarios A, A2 and B (see Section 2), must therefore be explicitly resolved for each tidal energy site resolve in the global data (Section 3.3). Nevertheless, the uncertainty of optimal rated speed (*Vr*) is clear in Figure 7 as the divergence of the optimal power-density curve (described as relative rated turbine speed Vr/UM2) for maximum and high yield (Scenario A and A2) or firm power (red line of Scenario B) as the F value increases and the tidal dynamics change from a regular semi-diurnal (F value<0.25) to a mixed (between 0.25 and 3) or diurnal (F value>3) system (i.e. one tide per day tide).

3.3. Optimal power curve analysis for the world

Spatial variability of tidal dynamics are shown in Appendix A2 as details from data are not clear. The variability of global tidal dynamics is shown in Figure 8 relative to resource, calculated here as maximum tidal current speed (maxU) using the sum of the four major tidal dynamics M2, S2, K1 and O1. Probability exceedance (Prob Exc.) of resource (maxU) resolved in FES2014 data up to 25 km from a land mass is shown in Figure 8a; ~12.8% of sites have maxU>1 m/s, 3.6% of sites have maxU>1.5 m/s, ~1.1% sites have maxU>2 m/s and ~0.3% of global sites resolved have maxU>2.5 m/s. The majority of sites have a dominant M2 current amplitude ~70% of maxU; however some potential tidal energy sites (e.g. maxU>2m/s) have a much lower M2 contribution (see Figure 8b), which can also be seen in Figure 8c. Grouping the tidal data of Figure 8c: 53% of sites resolved had F value below 0.25 (semi-diurnal tides) and 46% were "partial" (F value between 0.25 and 3), with relatively large contributions of K1 and O1 constituents. Some "high tidal resource" (e.g. maxU>3 m/s) of Figure 8c exhibit F values above 3 (one tide per day), but account for ~1% of the sites resolved. Figure 8 therefore indicates tidal dynamics at potential tidal-stream energy sites, and thus the temporal variability of resource, will vary greatly around the world, and any analysis that considers low flow sites (e.g. maxU<2.5 m/s) will have an exponentially greater number of sites with varying tidal dynamics to consider (see Figure 7).

Applying the standardised power curve method (see Section 2), the optimal rated turbine seed (*Vr*) for Scenarios A, A2 and B were computed (e.g. shown for an idealised tide in Figure 7), and are shown in Figure 9. Optimal rated tidal-stream turbine speed (*Vr*) using

global data is shown in Figure 9 as absolute (Fig. 9a) and as a percentage of annual maximum tidal current speed (Fig 9b). Both maximum (scenario A) and high (scenario A2) optimisation solutions showed little variability with the exception of low resource sites (where maximum current speed was below 1m/s), with a good linear regression fit (panel a) and small standard deviation (shaded region of panel b) of Figure 9 (values given in Table 2). Optimal *Vr* for Scenario B (firm power) had a large amount of variability and some trend apparent with tidal resource (Table 2 and Figure 9), likely because the result was greatly affected by tidal form (i.e. the relative contribution of diurnal constituents K1 and O1).

Annual maximum current speed (maxU) was based on the peak current speed simulated at a given site in 2020 using the sum of four tidal constituent amplitudes (e.g. UM2), calculated the major axis length of each tidal constituent ellipse (CMAX), i.e.

$$maxU = UM2 + US2 + UK1 + UO1 = \sum^{m2,s2,k1,o1}(Cmax) \text{ [8].}$$

Hence, optimal rated speed for maximum yield (Scenario A) will below 100% of maxU as this rarely occurs (when the four considered constituents are in-phase). Two measures of *Vr* are given (% of max U and absolute). The linear regression statistics, and discretised mean *Vr* (as % of maxU) for grouped site current speeds, are given in Table 2 alongside respective performance metrics of the mean trend line fit (RSQ for absolute) and Pearson correlation (RHO) – associated P-value is not shown as all <0.001 at 5% significance. The standard deviation (STD of Table 2) and convergence of shaded area in Figure 9b show variability in an optimal rated turbine speed (relative to resource), and clear convergence can be seen in the optimal yield scenarios (Scenarios A and A2).

Optimal rated speed (*Vr*) for scenario B (firm power) varied with resource (i.e. current speed climatology at a site); with relative mean *Vr* found to increase with maximum current speed (see Figure 9 and Table 2) but with a similar amount of variability (STD of Table 2). This increase in scenario B relative rated turbine speed (*Vr* as % of maxU) is likely the significant decrease in sites resolved when increasing maxU (see Figure 8a) as well as the tendency for a semi-diurnal (Fig 8b) and dominant M2 amplitude (Fig 8c) in the tidal dynamics. Furthermore, spatial variability in Scenario B was found when *Vr* (relative to maxU) were grouped into 6 continents - see Table 3 and are shown in Appendix (Figure A3). Therefore, our analysis shows an optimal tidal-stream turbine rated speed (*Vr*) based on firm power supply – spatially varies due to the nature of the tide and the magnitude of the resource.

4. Discussion

Complex analysis involving a large amount of data resulted in a simple set of rules researchers and engineers can use in renewable energy resource assessment:

(1) Tidal-turbine cut-in speed (*Vs*) was found to be ~30% of rated turbine speed (*Vr*) on average;

(2) For a deployment concerned with near-maximum yield aspirations, rated tidal-stream turbine speed (*Vr*) at a given site will be ~87% to 97% of site maximum flow respectively (where max flow is assumed as the sum of current speed amplitude of M2, S2, K1 and O1 constituents: see Robins et al., 2015), with little global variation found;

(3) Deployments concerned with firm, constant power and small amounts of storage, may aim to deploy tidal-stream turbines with much lower rated speeds (~56% of site maximum flow), with spatial variability due to resource (maximum current speed) and the tidal form (F value) – due to the nature of the tide at a given site (see Robins et al., 2015);

(4) Average values of normalised data from fourteen horizontal axis tidal-stream turbines (Table 1), alongside our estimation of optimal cut-in and rated speed, allows a standardised power curve and device behaviour (Figure 3) to be implemented in resource and environmental impact assessment, without bias to one specific design (e.g. Fairley et al., 2020) to allow tidal energy resource mapping for future technologies (e.g. Lewis et al., 2015).

To ensure the result is not affected by the tidal harmonics data, the analysis of the two scenario extremes (maximum yield and firm power: Scenarios A and B) were compared to the result from tidal data at higher resolution: latitudinal resolution of 1/100°(~1 km) instead of 1/16°(~7 km) in the FES2014 global data. The higher resolution tidal data was taken from the Robins et al. (2015) hydrodynamic model of a UK domain (14°W to 11°E, and 42°N to 62°N), using the same four tidal constituents (M2, S2, K1 and O1) computed from a 30 day simulation. FES2014 data were interpolated to the Robins et al. (2015) computational grid and domain, and *Vr* optimisation (of section 3.3) repeated; the comparison of the optimisation algorithm, using tidal harmonic data from these two spatial resolutions, is shown in Table 4.

To compare sensitivity of turbine optimisation to tidal model data accuracy (Table 4), Root Mean Squared Error (RMSE) and Linear Regression score (RSQ) were estimated assuming the higher resolution data accurate, alongside Scatter Index and the mean downscaling value to convert between model spatial resolutions (e.g. M2 amplitude of coarse data was 66% of the higher resolution model on average). Therefore, the tidal resource data may differ between the two model resolutions (coarse data under-predicting flow speed), but the optimal rated turbine design was found to be constant and independent of tidal flow speed (see Table 4) likely because the relative size of the four tidal constituents, used in this study, slowly spatially vary whilst tidal current magnitude is enhanced by bathymetry – and thus dependant on model spatial resolution.

Indeed, the tidal data sensitivity test (Table 4) showed that although spatially coarse data under-predicted tidal current speeds (both maximum and the main M2 constituent – see Table 4), the optimal rated turbine speed (*Vr as a % of maxU*) was independent of tidal data resolution. Anecdotal verification of optimal turbine rated speed, using the coarse data, can be assessed by comparing our optimal rated speed result to an industry driven solution; for example, the Meygen site (Pentland Firth) has a maximum current speed ~3.5m/s (Goward-Brown et al., 2017) giving an estimated rated speed (*Vr)* of 2.9m/s to 3.4m/s (for A2 and A: high to maximum yield scenarios), which is very close to the 2.65m/s to 3.05m/s turbines installed at the site (e.g. Website 2) especially given the extremely coarse global tide data (~7km spatial resolution).

It is likely that the relative magnitude of the major tidal constituents (i.e. excluding over-tides such as M4), which describe tidal form (F value), has low spatial variability (e.g. Robins et al., 2015; Lewis et al., 2017); therefore, tidal dynamics (i.e. nature of tide) are resolved in coarse models as spatial variation is small, but tidal current amplitudes are under-predicted because coarse models do not resolve bathymetric features that accelerate tidal currents (see Lewis et al., 2015). Therefore, coarse resolution tidal data can be used to resolve tidal dynamics, but not the magnitude of theoretical tidal-stream energy resource – hence, future resource mapping efforts must be based on high resolution tidal data (also concluded in Lewis et al., 2017). Higher tidal harmonics (such as the combination of M2 and M4, leading to overtides and flood-ebb asymmetry) can have a significant effect on resource assessment (Neill et al., 2014), and are enhanced by tidal-stream turbine deployments (e.g. Neill et al., 2009), whilst interaction of array-scale tidal energy developments must be included within resource assessment (e.g. Garrett and Cummins, 2008; Vennel et al., 2015); therefore, we hope the standardised power curve presented here will lead to improved understanding of tidal-stream energy potential.

The approach taken to provide a standardised power curve for use in tidal-stream resource assessment, builds on the work of Hardisty (2012) in the application of an idealised tidal-stream power curve, and device technology reviews of Roberts et al. (2016) and Zhou et al. (2017). In the technologically mature wind energy industry (Lydia et al., 2014), there is reported convergence in wind turbine cut-in speeds (due to insufficient torque to initiate

turbine rotation at wind speeds lower than 3m/s) and rated speeds (11-17 m/s), although some variability in design depending on local wind conditions (Carrillo et al., 2013). The knowledge of a common power curve in the wind industry has supported mean resource assessment with much research now focusing on finer-scale variability (Trivellato et al., 2012; Lydia et al., 2014). Therefore, our simple set of tidal turbine power curve rules, set out in this paper, would allow improved resource and impact assessments with hydrodynamic models.

Given the deterministic predictability of tidal-stream resource, and the establishment of a standardised and resource-led power curve (presented here), a convergent tidal-stream energy power curve should be the focus of future research to aid resource mapping (e.g. ”mhkit”; website 4). If we apply technology development of tidal-stream energy (based on Lewis et al., 2015): 1st to 3rd generation sites have peak flow speeds >2.5m/s, 2m/s, and 1.5m/s respectively. Applying the high yield optimisation (Scenario A2) to the global tidal data: 1st generation devices should be considered having rated speeds above 2.2 m/s (*Vs* ~ 0.7 m/s), with 2nd generation rated speed above 1.7 m/s (*Vs* ~0.5 m/s) and 3rd generation rated speed above 1.3 m/s (*Vs* ~0.4 m/s); close to the 0.5 m/s current speed threshold to initiate turbine rotation (Encarnacion et al., 2019).

Technological learning has led to a reduction in the cost of wind energy devices (Junginger et al., 2004), and a similar cost reduction is expected for tidal energy (Johnstone et al., 2013). Our analysis confirms tidal turbine rated speed optimisation can be achieved. The inclusion of swept tidal-stream turbine area, alongside economies of scale, practical and socioeconomic constraints (e.g. Vazquez and Iglesias 2015), would therefore allow for a convergent resource-optimised tidal turbine design and cost assessment. However, future research must resolve uncertainties in array design choice (e.g. Coles et al.,, 2020); for example, resolving cost of optimised device resilience (maintenance) and yield, will one turbine be installed throughout a country, region or array?

The predictability of tidal energy, compared to the temporal variability of other non-thermal renewable energy resources (see Lewis et al., 2019) and the analysis presented here, indicates the need for develop tools that can perform “whole systems” design of renewable energy systems – where the storage costs and dispatchability of power included in supply-demand analysis (e.g. Stegman et al., 2017; Al Katsaprakakis et al., 2019) as well as resilience and reliability (Johnstone et al., 2013). As power is proportional to the cube of velocity (equation 1), challenges in competitive costed low-flow tidal turbines are clear (i.e. low yields will likely raise LCOE greatly). However, the potential for low-flow tidal energy devices appears great if we consider the persistence of power density achieved with a Scenario B power curve (gap in power <2hours with the highest Capacity Factor), the cost of storage and resilience in an off-grid energy solution: for example, Large lithium batteries (~$500/kWh Nielsen et al., 2018) and the use of back-up diesel generators (e.g. Mala et al., 2009).

Given the prevalence of lower tidal flow sites (e.g. Lewis et al., 2015; 2017), where turbulence intensity (Lewis et al., 2019) and less mean vertical shear (Lewis et al., 2017b) will improve resilience of devices (Encarnacion et al., 2019), the potential cost of low flow tidal-stream turbines appears an important future step. Applying the conservative “firm power” optimisation (Scenario B) to the global data: 1st generation devices would have a rated speed of ~1.5 m/s (*Vs* ~0.5 m/s), 2nd generation rated speed ~1.2 m/s (*Vs* ~0.4 m/s) and 3rd generation ~0.9 m/s (*Vs* ~ 0.3 m/s). Although all rated speeds in our Scenario B were above the 0.5 m/s threshold, novel turbine designs are will be needed to improve tip-speed-ratios of turbines at low current speed (0.5 m/s or below: Encarnacion et al., 2019). Indeed, our analysis finds ~12.8% of the world’s coastlines have maximum current speeds above 1 m/s (resolved in FES2014 up to 25km offshore and excluding high (> 70°) Latitudes), and 3.6% for maxU>1.5 m/s (see Figure 8 and Appendix A2); however absolute currents speeds

are known to be effected by ocean model resolution (Lewis et al., 2015; 2017) and this number is likely to be much higher. Therefore, higher resolution tidal resource data is needed to perform a full tidal-turbine device optimisation assessment, but the analysis presented here shows a suitable method once such data is available.

Previous research, using high resolution regional models, has shown less energetic flows dominate South East Asia (e.g. Encarnacion et al., 2019), such Malaysia (current velocities reaching up to 1.2 m/s Lim and Koh, 2010) and Philippines ("most areas reaching current velocities of 1.4 m/s" Encarnacion et al., 2019). The development of floating tidal-stream devices (Brown et al., 2020) has unlocked the potential for 2nd and 3rd generation tidal energy sites in the Gulf of California (where peak currents are between 1.0 and 2.4m/s, Mejia-Olivares et al., 2018), and the Kuroshio current where 1m/s to 1.5m/s oceanic currents could be harnessed with floating deep-water, large swept area devices (Liu et al., 2018). Indeed, low-flow rated (1.3 m/s to 1.7 m/s) tidal energy kites, with a large swept area, are also being tested and deployed (Buckland et al., 2015; Roberts et al., 2016). However, there is still a gap in low flow tidal turbines for lower power demand markets and "blue growth economies" (LiVecchi et al., 2019). For example, incorporation of tidal energy into offshore aquaculture would require tidal-stream devices capable of operating in <1m/s flows (see Gentry et al., 2017), and although some bio-optimisation to accelerate tidal currents is possible (O'Donncha et al., 2017) it may not be required given modest power needs (Aquatera 2014). We therefore, find two tidal-stream turbine markets and designs may be found in the future: (1) larger MegaWatt scale electricity production for grid-connected regions and (2) smaller-scale power systems that provide firm energy for higher value, remote industries and communities.

5. Conclusion

Given the sparsity of published power curves in the literature, and the diverse range of markets tidal energy could benefit, an unbiased power curve characterisation is essential to map tidal-stream energy resource. A standardised tidal-stream power curve was developed so that resource assessment beyond realised technologies can be possible. Our analysis and resource-led optimisation was unaffected by tidal data; finding divergence in rated-speed based on weighting of importance: firm power with low amounts of storage, or high yield with larger storage needs. A general rule for turbine power curve of a horizontal-axis turbine was found: cut-in speed was around 30% of the rated speed; and optimal rated speed (tidal current when peak power converted) was either ~50% or greater than 87% of a site's maximum current speed (based on sum of M2, S2, K1 and O1 harmonic constituents) for firm power or maximum yield respectively - due to the dominance of the major semi-diurnal lunar tidal constituent (M2). This paper demonstrates the "power" of deterministic predictability with tidal energy, and although temporal variability of the tidal resource appears to be captured by current tidal data products, higher resolution data could transform the tidal-stream energy industry by fully mapping the resource. This work also adds to the weight of evidence that a convergent tidal turbine design is needed, and possible, but two tidal-stream turbine types may exist: one for electricity supply to large grid connected communities, and another "lower resource" turbine for remote industry and communities that may have much lower rated speeds.

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8. Figure Captions:

Fig 1. A demonstration of the effect of two tidal power curves on resource assessment. A spring-neap time-series (2m/s M2 Cmax and 0.5m/s S2 Cmax) of tidal current speed (panel a) is converted to theoretical power density (PD) in panel b and technical power density (panel c) for a power curve rated at 2.5m/s (red line) and 2.0m/s (blue line).

Fig 2. Tidal-stream turbine characteristics from 14 commercially developed devices (panel a), normalised (relative to rated power and speed) and compared to observed variability (grey dots and averaged power curve in red) from a grid-connected device in Lewis et al. (2019).

Fig 3. A standardised power curve, based on 14 horizontal axis tidal-stream turbines, with the associated Drag (as percentage of maximum drag, Dr) and Thrust Coefficient (CT) normalised curves.

Fig 4. Single harmonic tidal current (M2 amplitude 2 m/s) over a 2 day period (panel a), and the theoretical power density (PD) of this current (panel b), compared to the mean power density and Capacity Factor (panel c) for multiple tidal-stream turbine power curves, where rated power is capped at rated speed (Vr, and cut-in speed is 30% of Vr), which allows mean daily yield density to be calculated (panel d).

Fig 5. Spring-Neap tidal current (M2 amplitude 1 m/s, S2 amplitude 0.6 m/s) over a 7 day period (panel a), with the theoretical power density (PD) of this current (panel b). Multiple tidal-stream turbine power curves, where rated power is capped at rated speed (Vr, and cut-in speed is 30% of Vr), are applied to resolve an optimal design using mean power density and Capacity Factor (panel c) and mean daily yield density (panel d).

Fig 6. Performance of multiple tidal-stream power curves, represented here as rated speed (*Vr*) relative to the resource (amplitude of M2 harmonic: *UM2*), for a given site where the tidal currents are controlled solely by the spring-neap cycle and the ratio of M2 and S2 amplitude (M2/S2 of 0 has only an M2 tide, whilst equal M2 and S2 current amplitudes has a ratio of 1). Turbine performance is described using Capacity Factor (a), percentage of time no power produced (b), (c) mean yield density (relative to maximum possible) and (d) the longest period of zero power in a 15 day time-series.

Fig 7. Tide currents harmonic characteristic tidal form (F value), rated turbine speed (relative to M2 current amplitude UM2) and subsequent yield and Capacity Factor (CF) shown in panel a, with mean monthly percentage of zero power and maximum period of no power (max gap) in panel b. Lines of optimal power curve shown in solid white for selection of maximum yield (Scenario A), high yield (scenario A2) as dashed white line and firm power (power gap < 2 h with highest CF: scenario B) as red dashed line.

Fig 8. Global variability of tidal dynamics, described as maximum flow (maxU) percentage exceedance (a) for sites "coastally" (<25 km offshore) resolved in the FES2014 data, (b) coloured percentage occurrence of M2 amplitude contribution to the maximum flow (as percentage of M2 current amplitude compared to maximum

current speed), and (c) coloured percentage occurrence of the tidal form (F value) that describes the diurnal (F>3) to semi-diurnal (F<0.25) nature of the tide

Fig 9. Rated tidal-stream turbine speed using standardised power density curve and three optimal solutions: Scenario A (maximum yield density shown in black), Scenario A2 (high yield density shown in blue) and Scenario B (firm power shown in red).

Appendix

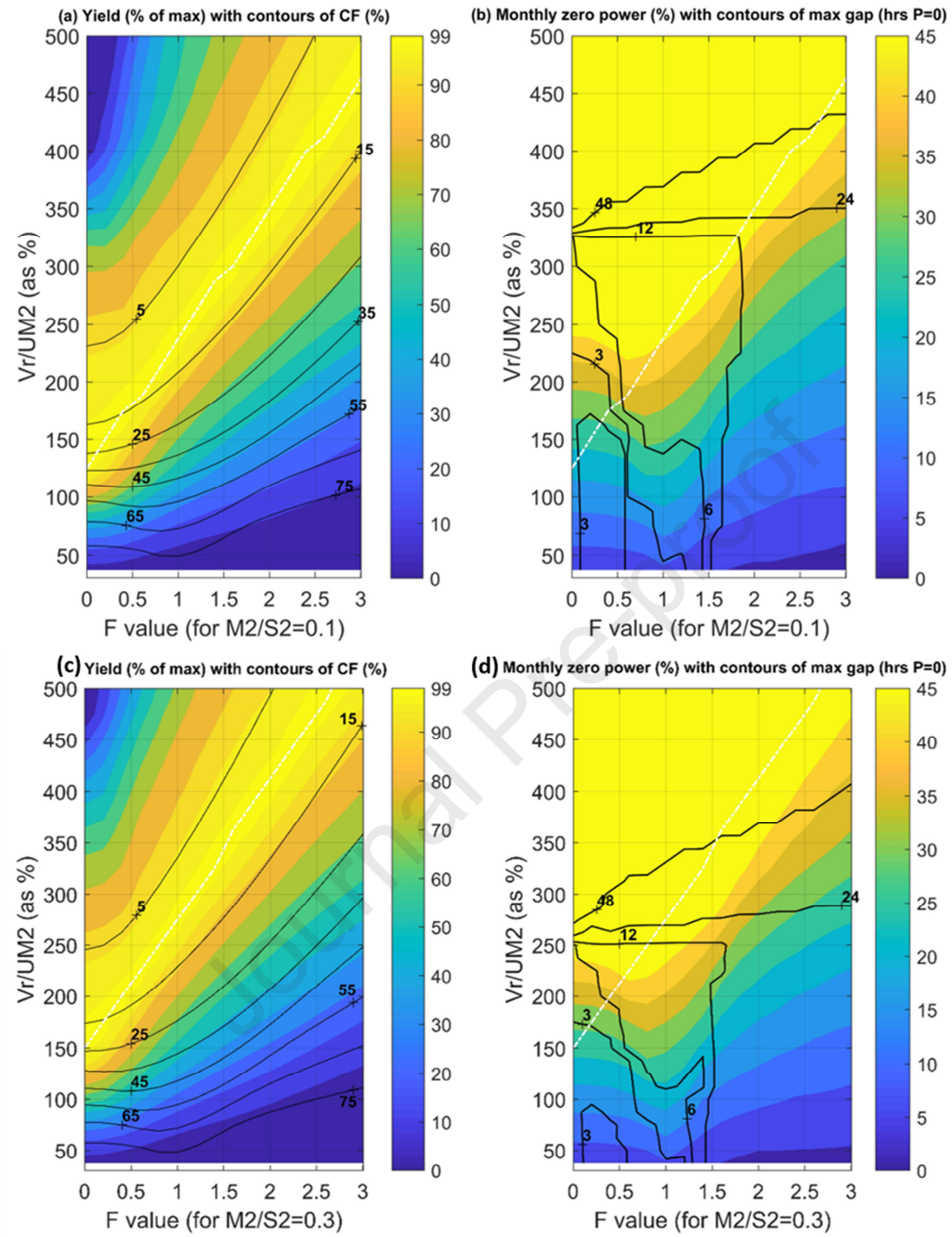


Fig A1. An example of sensitivity to the tidal-stream turbine optimisation result of Figure 7, when considering tidal dynamics with different M2/S2 ratios but equal F values. Tide currents harmonic characteristic tidal form (F value), rated turbine speed (relative to M2 current amplitude UM2) and subsequent yield and Capacity Factor (CF) shown in panel a and c; with mean monthly percentage of zero power and maximum period of no power (max gap) in panel b and d

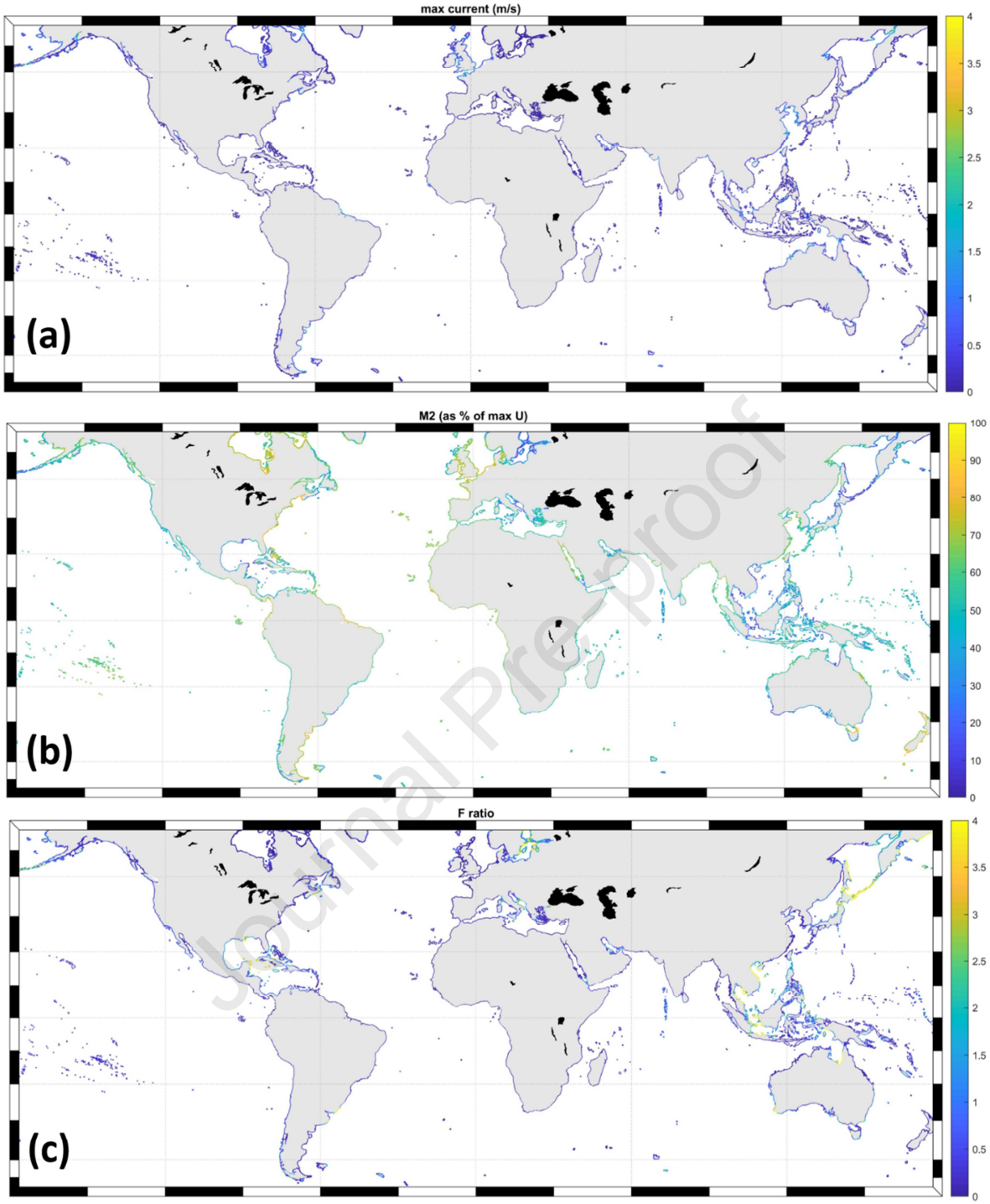


Fig A2. Global tidal dynamic variability, described as: (a) maximum current speed; (b) percentage of M2 current amplitude compared to maximum current speed; and (c) Tidal form (F-value) using FES2014 data

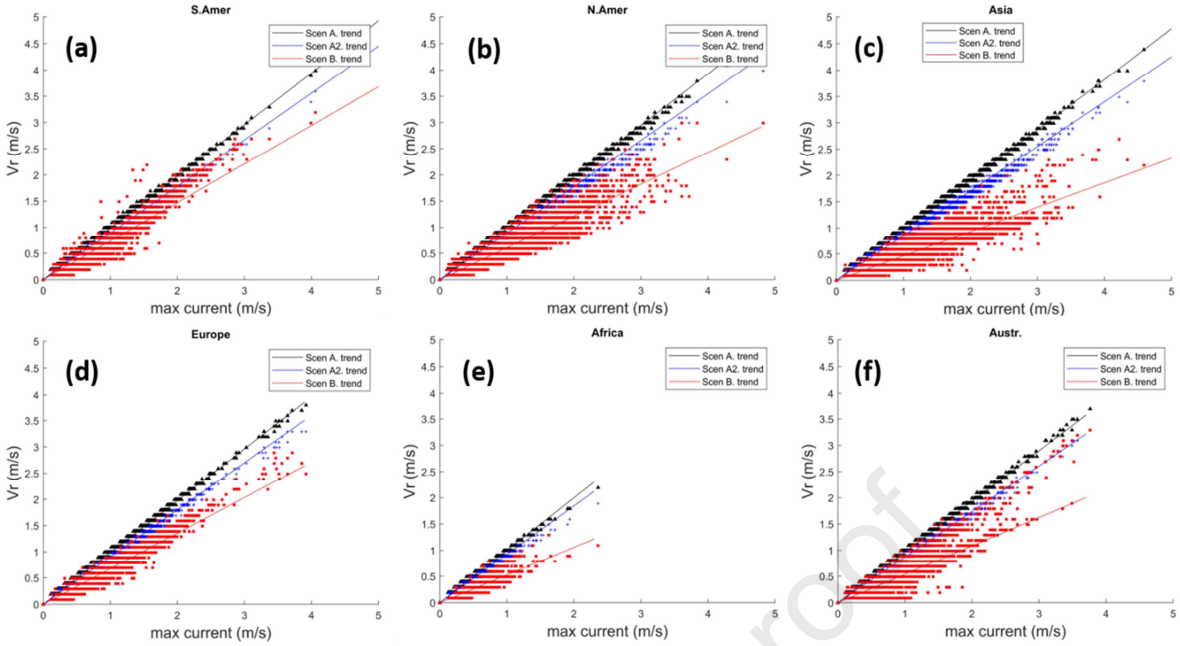


Fig A3. The optimal rated tidal-stream turbine speed, for three scenarios (a to c for max, high and firm yield respectively), based on FES2014 global data and grouped into the 6 continents: South America (a), North America (b), Asia (c), Europe (d), Africa (e), Australasia (f).

Table 1. A literature review of 14 horizontal axis tidal-stream turbines, where device characteristics are published or estimated (marked with *), including: rotor diameter (∅); Rated Power (Pr); power coefficient (C*p*); cut-in velocity (*Vs*) when the turbine starts to produce power; and rated velocity (*Vr*), the current speed when maximum power (*Pr*) is produced. Labels of devices in Fig. 2 are defined in the ID column.

ID	device	∅ (m)	*Pr* (kW)	*Vr* (m/s)	*Vs* (m/s)	*Vs* (as % of *Vr*)	*Cp**	source
1	**MCT**	16	600	*2.5*	*1*	*40*	*0.37*	Lewis et al. (2015)
2	**Alstrom**	18	1000	*2.7*	*1*	*37*	*0.39*	Lewis et al. (2019)
3	**sabella D-10**	10	1000	*4*	*1*	*25*	*0.39*	Website 1
4	**sabella D-15**	15	2300	*4*	*1*	*25*	*0.4*	Website 1
5	**seagen-S 2MW twin rotor**	20	1000 (per rotor)	*2.5*	*1*	*40*	*0.4*	Website 2
6	**Atlantis AR1000**	18	1000	*2.65*	---	---	*0.41*	Website 2; Roberts et al. (2016)
7	**Atlantis AR2000**	22	2000	*3.05*	*<1*	---	*0.36*	Encarnacion et al. (2019); Website 2
8	**Verdant gen5**	5	35	*2.59*	---	---	*0.32*	Polygae et al (2010); Encarnacion et al. (2019)
9	**Nova**	8.5	100	*2*	*0.5*	*25*	*0.43*	Encarnacion et al. (2019)
10	**Voith**	16	1000	*2.9*	---	---	*0.4*	Roberts et al. (2016)
11	**openhydro**	10	200	*2.5*	---	---	*0.32*	Polygae et al (2010); Roberts et al. (2016)
12	**schottel hydro d3**	3	70	*3.7*	*0.9*	*24*	*0.38*	Website 3
13	**schottel hydro d4**	4	62	*3.1*	*0.8*	*26*	*0.32*	Website 3
14	**schottel hydro d5**	5	54	*2.6*	*0.7*	*27*	*0.31*	Website 3
	Mean	**13**	**816**	***2.91***	***0.88***	***30%***	***0.37***	
	Standard Deviation	6	**803**	***0.6***	***0.18***	***7%***	***0.04***	

Table 2: Optimal rated tidal-stream turbine speed (*Vr*) relative to maximum tidal current speed (MaxU) at any given "coastal" site globally for three optimal power scenarios, with two methods of representing Vr: absolute with linear regression of max U and Vr (with linear regression score: RSQ), and Vr relative to maxU at site, discretised into 0.5m/s groups with mean Vr (as % maxU) and associated standard deviation (std), with the Pearson correlation score (RHO) is given to indicate strength of statistical fit at 5% confidence

		Optimal *Vr* scenario:		
		Max yield (scenario A)	High yield (scenario A2)	Firm power (scenario B)
Absolute *Vr* trend	RSQ	~100%	~100%	92%

	trend	*Vr* = 0.97*maxU	*Vr* = 0.87*maxU	*Vr* = 0.56*maxU
Mean *Vr* (as % of maxU) with standard deviation in brackets (std)	maxU	*Vr* as % of maxU (std)		
	0.5m/s	107 (17)	102 (17)	49 (13)
	1.0m/s	99 (8)	93 (9)	48 (17)
	1.5m/s	97 (4)	87 (4)	57 (16)
	2.0m/s	96 (3)	86 (4)	59 (15)
	2.5m/s	96 (2)	85 (4)	58 (16)
	3.0m/s	96 (2)	84 (3)	58 (16)
	3.5m/s	96 (2)	84 (3)	60 (17)
	4.0m/s	96 (2)	85 (3)	64 (16)
	4.5m/s	96 (2)	84 (3)	67 (12)
	RHO	-0.28	-0.43	0.24

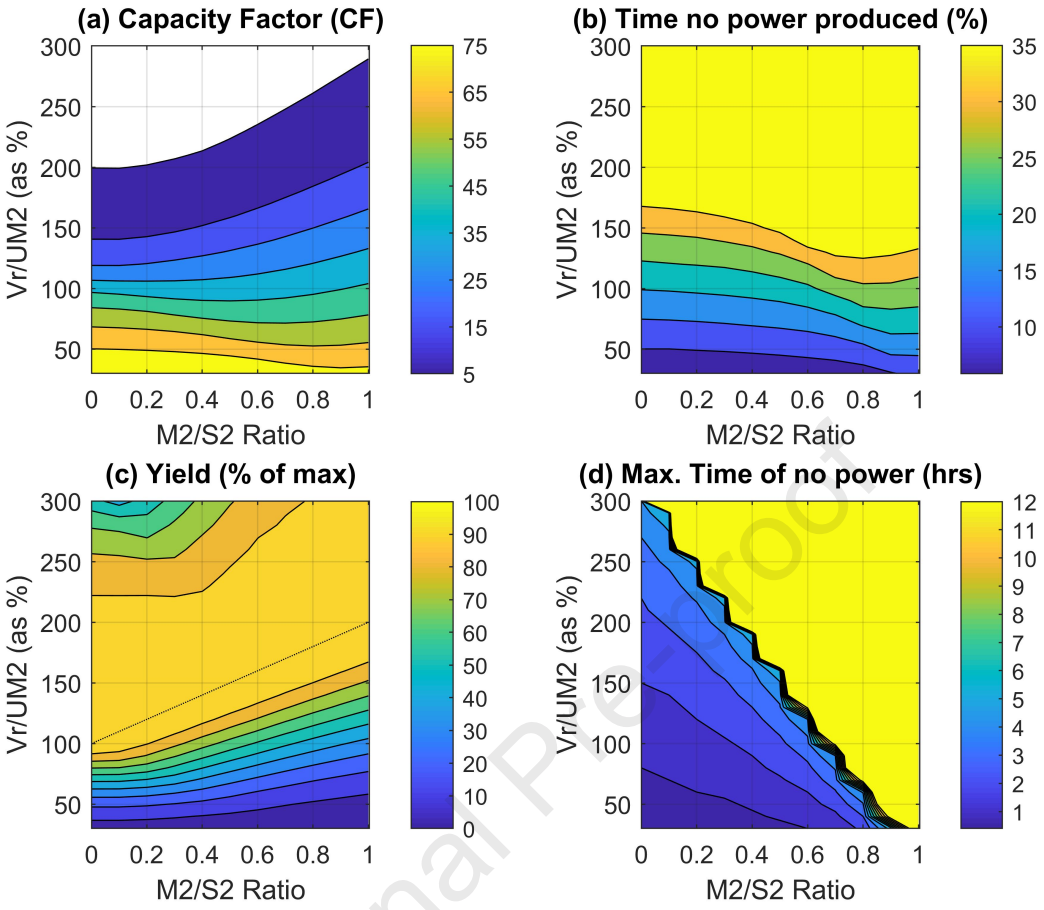
Table 3: The linear trend of optimal absolute rated turbine speed ("Trend" Vr in m/s), with each respective linear regression score (RSQ), for three tidal-stream energy scenarios (A , A2, and B) and spatially grouped data by continent, using four major tidal constituents of FES2014 data (latitude <70° and up to 25km offshore)

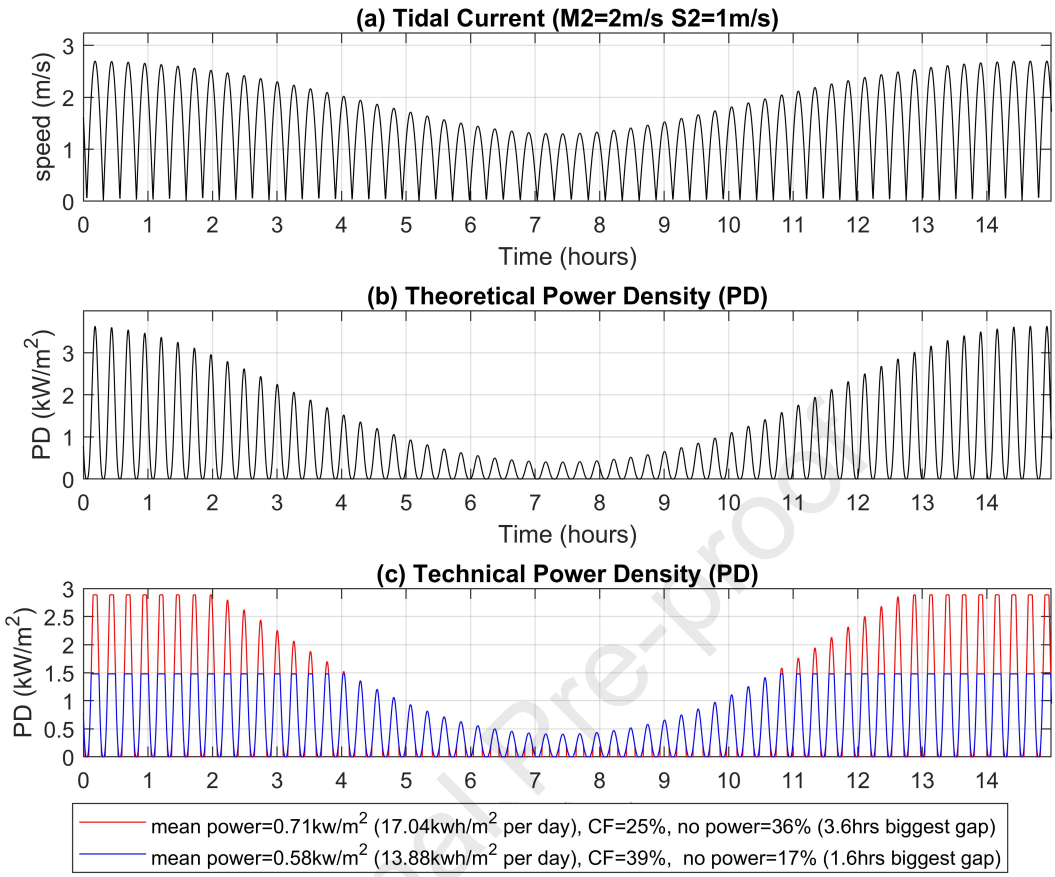
region	Scenario:	A (max yield)	A2 (high yield)	B (firm power)
World	RSQ	100%	100%	92%
	Trend	*Vr*=0.97*maxU	*Vr*=0.87*maxU	*Vr*=0.56*maxU
Europe:	RSQ	100%	100%	93%
	Trend	*Vr*=0.96*maxU	*Vr*=0.85*maxU	*Vr*=0.46*maxU
Australasia:	RSQ	100%	100%	91%
	Trend	*Vr*=0.97*maxU	*Vr*=0.87*maxU	*Vr*=0.54*maxU
Asia:	RSQ	100%	100%	93%
	Trend	*Vr*=0.96*maxU	*Vr*=0.85*maxU	*Vr*=0.46*maxU
Africa:	RSQ	99%	99%	91%
	Trend	*Vr*=maxU	*Vr*=0.92*maxU	*Vr*=0.53*maxU
North America:	RSQ	100%	99%	95%
	Trend	*Vr*=0.98*maxU	*Vr*=0.89*maxU	*Vr*=0.61*maxU
South America:	RSQ	100%	100%	96%
	Trend	*Vr*=0.99*maxU	*Vr*=0.89*maxU	*Vr*=0.74*maxU

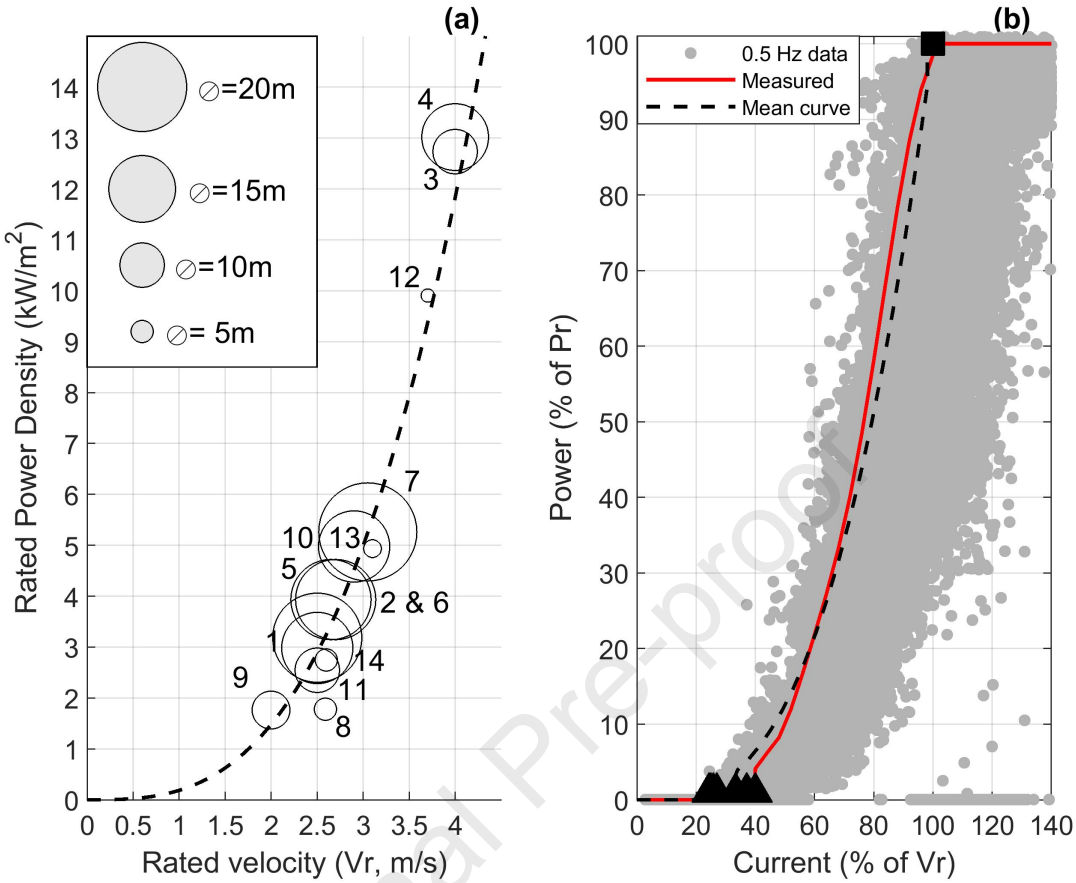
Table 4: Comparison of optimal tidal-stream turbine rated speed (Vr) based on two scenarios (max yield and firm power; scenarios A and B respectively) using tidal harmonic data, giving peak current speed as the sum of the four major constituents (K1,O1,S2,M2), called maxU, as well as the amplitude of current speed for the M2 constituent (Ua), for high and coarse spatial resolution (Res.) model data comparison for the UK region. Comparison metrics: Root Mean Squared Error RMSE) and linear regression score (RSQ) provided alongside scatter and average conversion between resolutions.

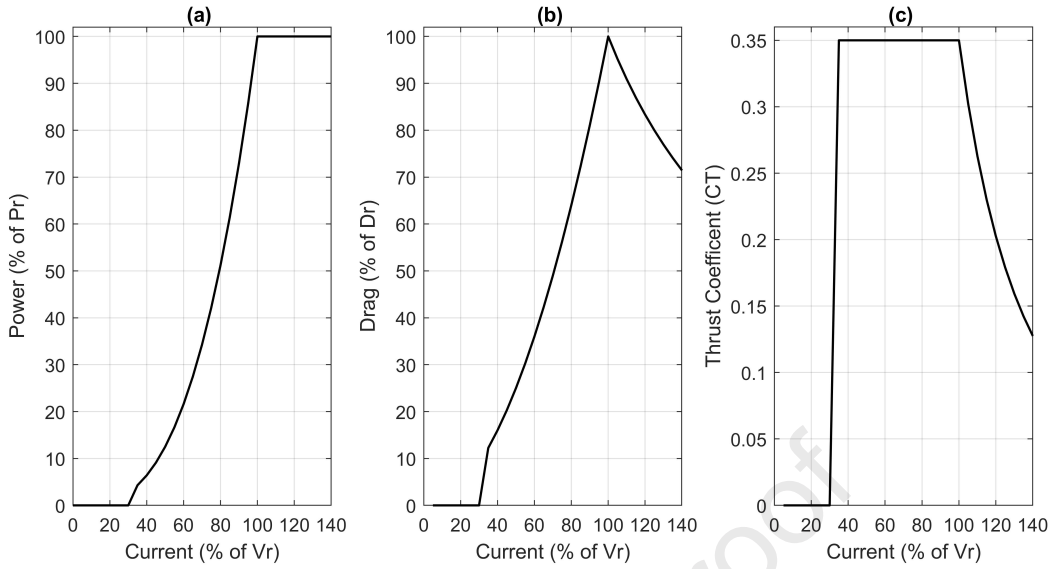
	High res. Robins et al. (2015) (~1km spatial	**Coarse res. FES2014 (~7km resolution)**

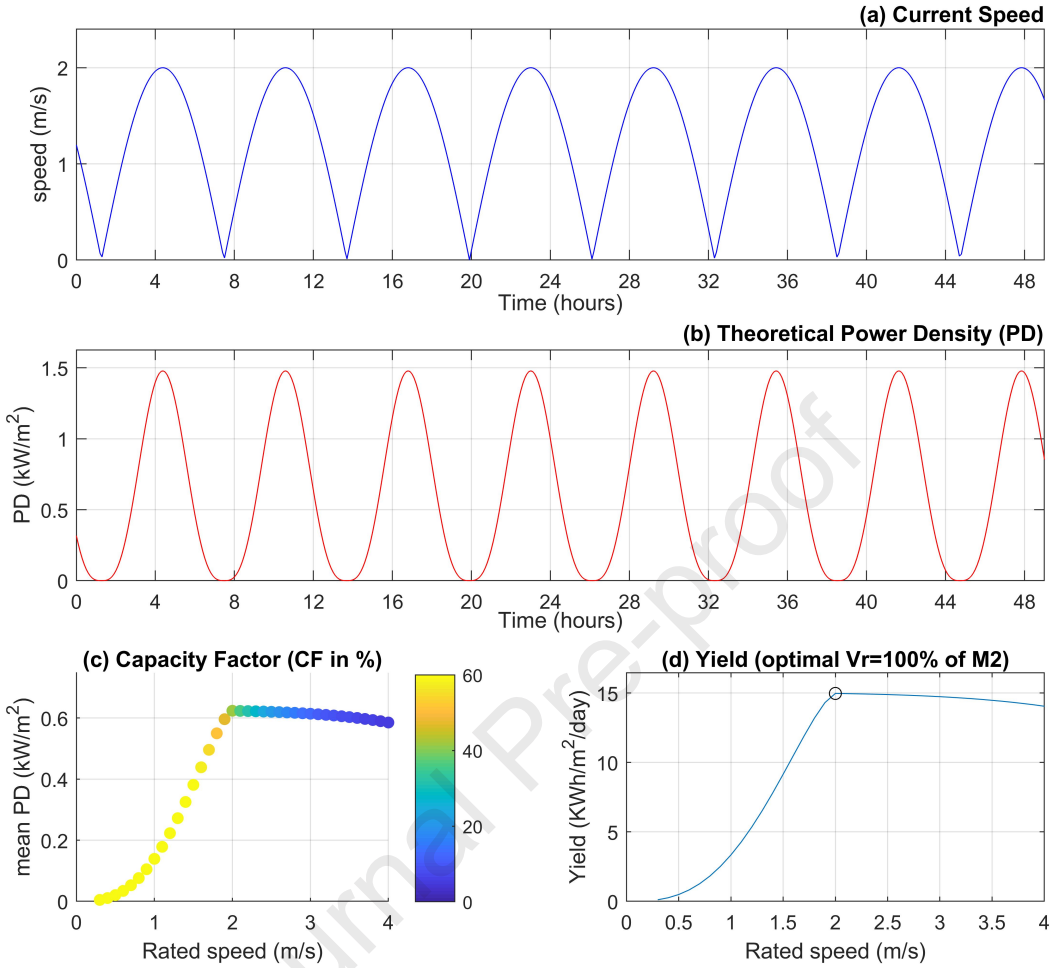
	resolution)
Scenario A linear trend: **Scenario B linear trend:**	**Vr~0.97maxU+0.01** **Vr~0.98maxU** **Vr~0.58*maxU+0.05** **Vr~0.56maxU + 0.27**
M2 current amplitude comparison:	**RMSE = 0.18 m/s (4%)** **RSQ = 71%** **Scatter Index = 31%** **Coarse(Ua) ~ 0.66*high(Ua)**
Maximum current comparison:	**RMSE = 0.23 m/s (4%)** **RSQ = 71%** **Scatter Index = 28%** **Coarse res. (maxU) ~ 0.68*high res. (maxU)**

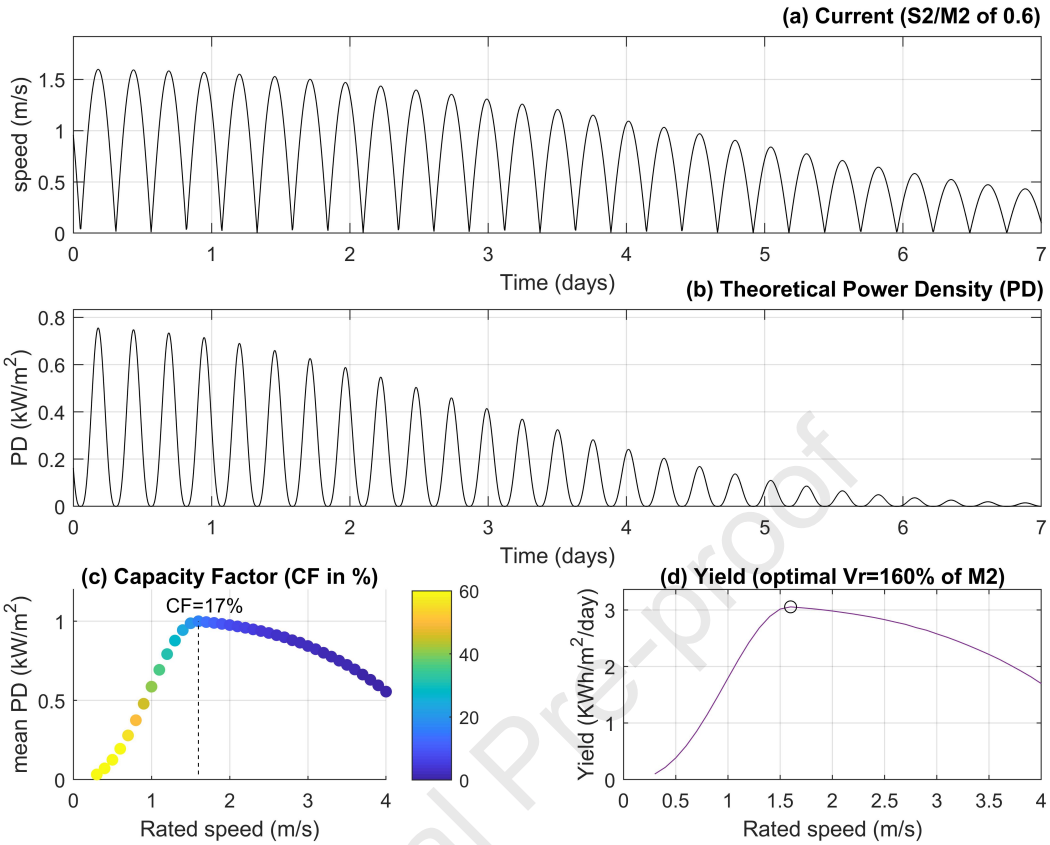


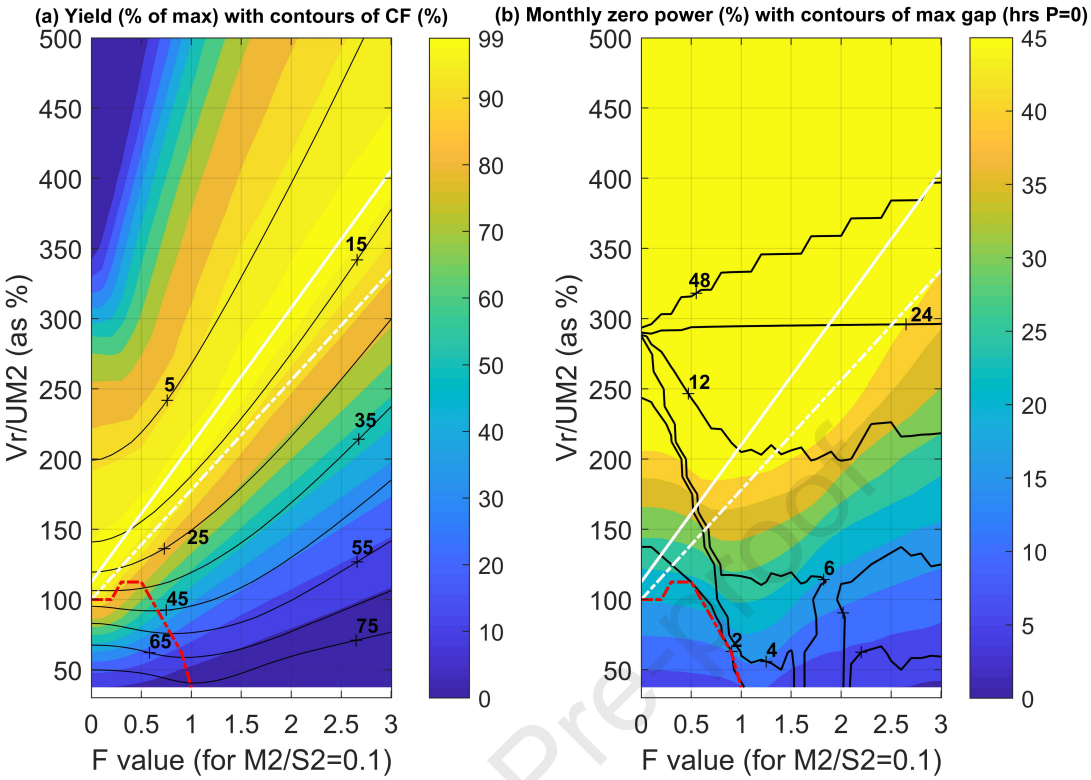


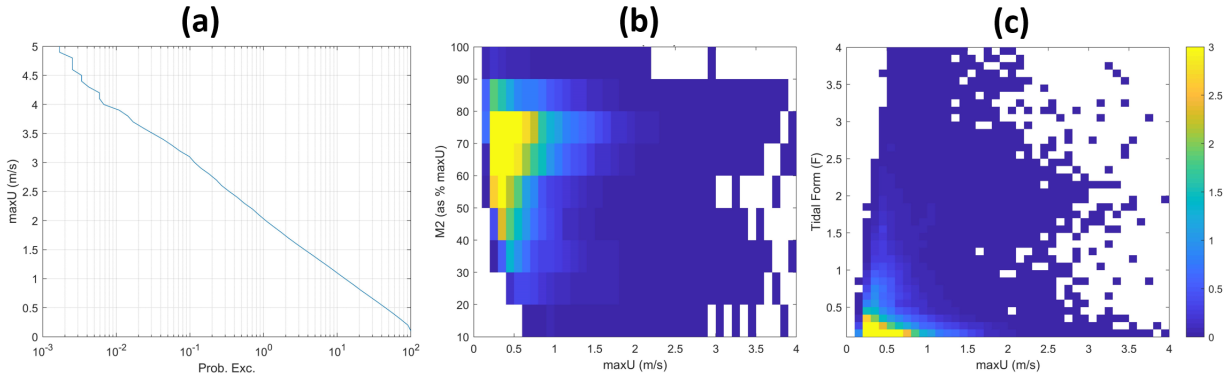


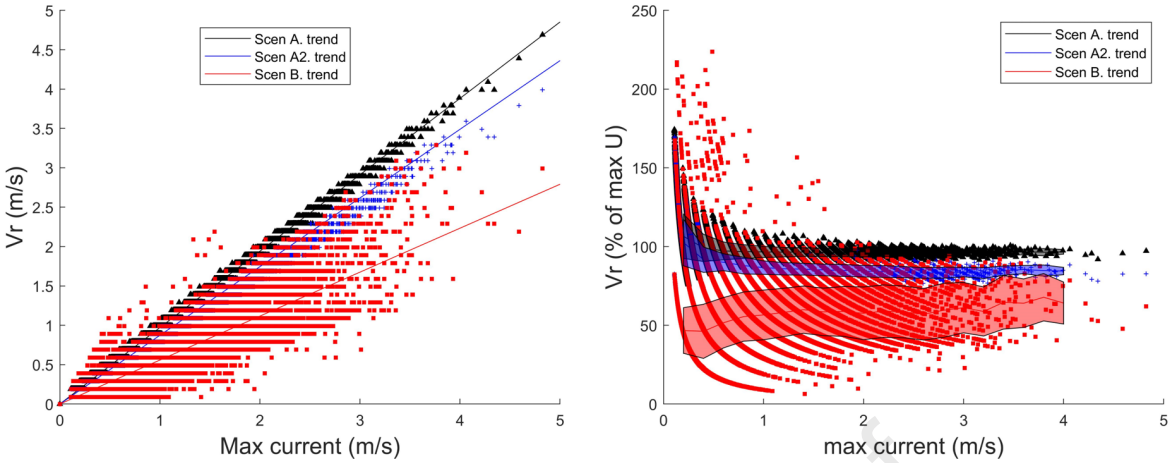












Highlights:

- **Standardised horizontal-axis tidal-stream turbine power-density curve developed**
- **Convergent power curve characteristics assessed with global tide data**
- **Divergence in rated-speed when selecting for optimal yield or persistent power**
- **Resource-led turbine optimisation is possible but high resolution tidal data needed**
- **High and low flow designs appear needed to capitalise on resource predictability**

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