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Ergodic Capacity and Error Performance of Spatial Diversity UWOC Systems over Generalized Gamma Turbulence Channels

Hongyan Jiang ^{1,2}, Hongbing Qiu ¹, Ning He ^{1,2}, Wasiu Popoola ³, Senior Member, IEEE, Zahir Ahmad ⁴, and Sujan Rajbhandari ^{5,*}, Senior Member, IEEE

- ¹ School of Information and Communication, Guilin University of Electronic Technology, Guilin 541004,
 China; qiuhb@guet.edu.cn, eicnhe@guet.edu.cn
- 8 ² Guangxi Key Laboratory of Wireless Broadband communication and Signal Processing, Guilin 541004, China; jianghy@guet.edu.cn
- School of Engineering, Institute for Digital Communications, University of Edinburgh, Edinburgh EH8
 9YL, UK; w.popoola@ed.ac.uk
- ⁴ School of Computing, Electronics and Mathematics, Coventry University, Coventry CV1 5FB, UK;
 ab7175@coventry.ac.uk
- School of Computer Science and Electronic Engineering, Bangor University, Bangor, LL57 1UT, UK;
 s.rajbhandari@bangor.ac.uk;
- 16 * Correspondence: <u>sujan@ieee.org</u>

17 Abstract: In this paper, we study the ergodic capacity (EC) and average bit error rate (BER) of spatial 18 diversity underwater wireless optical communications (UWOC) over the generalized gamma (GG) 19 fading channels using quadrature amplitude modulation (QAM) direct current-biased optical 20 orthogonal frequency division multiplexing (DCO-OFDM). We derive closed-form expressions of 21 the EC and BER for the spatial diversity UWOC with the equal gain combining (EGC) at receivers 22 based on the approximation of the sum of independent identical distributed (i.i.d) GG random 23 variables (RVs). Numerical results of EC and BER for QAM DCO-OFDM spatial diversity systems 24 over GG fading channels are presented. The numerical results are shown to be closely matched by 25 the Monte Carlo simulations, verifying the analysis. The study clearly shows the adverse effect of 26 turbulence on the EC & BER and advantage of EGC to overcome the turbulence effect.

Keywords: average bit error rate; ergodic capacity; generalized gamma; underwater wireless optical
 communications; spatial diversity; OFDM

29 1. Introduction

30 Underwater wireless optical communication (UWOC) is considered as an attractive 31 complementary solution to underwater acoustic communication due to its high data rate, low latency 32 and low implementation cost [1]. However, there are several challenges in implementing the UWOC 33 system due to the adverse channel condition caused by absorption, scattering and turbulence in the 34 oceanic environment [2]. There have been several attempts to establish a realistic channel model that 35 can accurately predict the performance of the UWOC [1]-[9]. The attenuation due to absorption and 36 scattering is well understood and mostly modelled by the radiative transfer equation [3], ray-tracing 37 simulations [4], and a closed-form expression by fitting simulation data [5]. Underwater optical 38 turbulence (UOT) caused by the variations in the refractive index due to temperature fluctuation, 39 salinity variations and the presence of air bubbles adversely affect the link performance [6]-[7]. Hence, 40 there has been significant attention to accurately characterize the UWOC turbulence channel to 41

41 predict the performance and establish mitigation techniques [8]-[9].

The early studies on the UOT channel adopted lognormal distribution which is commonly used todescribe atmospheric turbulence in free-space optical (FSO) system. However, the mechanisms of

44 turbulence generation in underwater and FSO channels are different and hence the lognormal 45 distribution does not accurately model the UOT in all the conditions [7]. Subsequently, several studies 46 of UOT have been carried out taking into account of several fading causes. In [10], a generalized 47 gamma distribution was proposed to describe the temperature-induced weak turbulence. In [11], it 48 was verified that Weibull distribution matches the measured data under all turbulence channels 49 caused by salinity gradient. However, it was shown in [12] that the measured data in the presence of 50 air bubbles do not fit well by a single-lobe distribution and required a two-lobe statistical model. 51 Taking into account both air bubbles and temperature gradient, an exponential-generalized gamma 52 (EGG) distribution model was proposed in [7] which excellently matches the experimental data under 53 all channel conditions. Using beam expander-and-collimator (BEC) at the transmitter side and/or 54 aperture averaging lens (AAL) at the receiver side, it was shown in [13] that the GG and exponential 55 Weibull distributions provide an excellent agreement with the measured data in UWOC channels 56 with random temperature and salinity variations in the presence of air bubbles, covering a wide range 57 of scintillation index values from weak to strong turbulence. In fact, GG distribution is a general case 58 of some of the important statistical distributions in modelling fading such as exponential, Rayleigh, 59 gamma, Weibull, Nakagami-*m* and lognormal [13]-[14].

60 It was established that turbulence-induced fading considerably increases the average bit error rate 61 (BER) and hence results in a large power penalty to achieve desired BER performance. This, in turn, 62 either significantly reduces the communication range or decreases the maximum achievable data rate. 63 To mitigate fading impairments, several techniques have been proposed, including a) error control 64 coding in conjunction with interleaving [15]-[16], b) maximum likelihood sequence detection [17], c) 65 multi-hop relaying transmission [18] and d) spatial diversity [19][20]. The first three approaches have 66 several practical limitations, namely large-size interleaves, high computational complexity and high 67 cost, but spatial diversity is not only the most practical and effective to mitigate the fading but also 68 reduces the possibility of temporal blockage by multiple apertures at the transmitter and/or the 69 receiver[21]. The spatial diversity scheme involves repetition coding at the transmitter and linear 70 diversity combining (LDC) technique at the receiver. There are three well-known LDC techniques, 71 namely maximal ratio combining (MRC), equal gain combining (EGC) and selection combining (SC). 72 Though MRC offers the best performance, it requires prior channel knowledge which is very difficult 73 to obtain especially for a time-varying channel[21]. Furthermore, the performance of EGC can match 74 very close to MRC for most practical cases [22]. Therefore, EGC is a more realistic option for practical 75 implementation due to its simplicity and low complexity [23].

76 The selection of the modulation scheme also affects the performance of UWOC in the oceanic 77 turbulence channel. The intensity modulation and direct detection with baseband modulation such 78 as On-Off keying (OOK) and pulse position modulation (PPM) are frequently used for UVLC due to 79 their simplicity and low cost. Though simple to implement, OOK needs adaptive detection to achieve 80 optimal performance in UOT channel [24]. PPM scheme, on the other hand, requires a very tight 81 pulse and symbol synchronization and has inferior bandwidth efficiency compared to OOK. The 82 subcarrier modulation (SCM) scheme is an alternative to the baseband modulation[25]. The SCM 83 permits the use of high-order constellations such as M-ary phase-shift keying (M-PSK) and M-QAM 84 by modulating an RF signal onto the intensity of the optical beam [26]. The OFDM is a special case of 85 SCM, where the carriers are orthogonal over one symbol period. OFDM offers high spectral efficiency, 86 resistance to inter-symbol interference and frequency selective fading[27][28]. To meet the real and 87 unipolar requirement of optical intensity modulation, several modified OFDMs were proposed, such 88 as DCO-OFDM, asymmetrically-clipped optical OFDM (ACO-OFDM), and asymmetrically clipped 89 DC-biased Optical OFDM (ADO-OFDM). DCO-OFDM is usually adopted in high bit rate 90 communication due to its high bandwidth utilization.

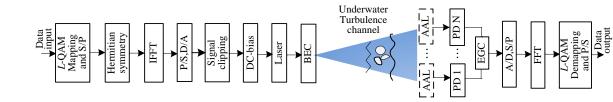
Although GG distribution has been shown to adequately model fading channels, there are very
 limited studies to evaluate the performance of various spatial diversity schemes over GG fading
 channels. Aalo *et al* derived the average symbol error rate performance of multilevel modulation

94 schemes for wireless communication systems in GG channels with diversity receivers [29]. Sagias et 95 al derived and evaluated union upper bounds for the outage and the average bit error probability for 96 ECG receivers[30]. In addition, Costa in [31] used another GG RV to approximate the sum of 97 independent identical distributed (i.i.d) GG RVs) and then derived the analytical expressions of 98 outage probability and average BER for the spatial-diversity wireless communication systems using 99 noncoherent frequency shift keying and noncoherent differential phase-shift keying. However, to the 100 best knowledge of the authors, there is no prior work to evaluate the ergodic capacity and average 101 BER of QAM-OFDM for spatial diversity UWOC systems over GG fading channels. Hence, in this 102 paper, we propose and study DCO-OFDM with a diversity scheme and EGC reception to mitigate 103 the fading and achieve high spectral efficiency. We derive a closed-form expression of average BER 104 based on the approximation of the sum of GG RVs and Gauss-Laguerre quadrature integrals. We also 105 derive the EC in terms of Fox's functions. Numerical results for average BER and EC of QAM DCO-106 OFDM with spatial diversity in the UWOC systems over GG fading channels are presented. The 107 results are further validated by Monte-Carlo (MC) simulations. To the best of our knowledge, this is 108 the first study of comprehensive mathematical derivation of the average BER and EC for DCO-OFDM 109 under turbulent UWOC.

110 The rest of the paper is organized as follows: Section II describes the UWOC channel in the presence 111 of UOT and DCO-OFDM with EGC diversity systems. In Section III, we derive the average BER and 112 EC. In Section IV, numerical and simulation results are presented, compared and discussed. Finally,

113 Section V concludes this paper.

114 2. UWOC system and channel model



115 116

Fig.1. The block diagram of the DCO-OFDM with diversity scheme for UWOC systems.

117 A block diagram of the proposed spatial diversity UWOC systems with DCO-OFDM scheme is 118 shown in Fig. 1. We consider one transmitter and N receiving apertures (the total area is the same 119 regardless of N) and standard modulation/ demodulation procedure of DCO-OFDM as described in 120 [32]. The information bits are modulated employing L-QAM scheme (where $log_2(L) > 0$ is an integer), 121 followed by a serial to parallel (S/P) converter. Before the inverse fast Fourier transform (IFFT) 122 operation, Hermitian symmetry is imposed on the OFDM symbol to generate a real-valued signal. 123 The outputs of IFFT operation are then serialized using parallel-to-serial (P/S) converter, followed by 124 conversion to analogue signals using a digital-to-analogue converter (DAC) and a filter. The real 125 signal is further converted to a unipolar signal to drive a linear optical modulator by clipping and 126 direct current (DC)-bias addition. The DC-bias level I_{DC} is given as Error! Reference source not 127 found.:

$$I_{DC} = g\sqrt{E_s} \quad , \tag{1}$$

128 where *g* is the normalized bias and E_s is the energy per symbol. The signal is pre-clipped at $\pm I_{DC}$ to 129 ensure a positive signal after addition of DC-bias [1].

Furthermore, the modulated beam is expanded and collimated to ease alignment. After propagating through the turbulence UWOC channel, the optical signal is received by photodetectors which can be equipped with AALs. EGC is adopted for the diversity scheme, and thus the total received instantaneous electrical signal is expressed as [17]:

4 of 14

$$y_{EGC}(t) = \sum_{i=1}^{N} y_i(t) = \eta I x(t) \sum_{i=1}^{N} \alpha_i h_i + n(t),$$
(2)

134 where η denotes the photodetector responsivity, x(t) represents the OFDM signal, I is the 135 irradiance, h is the path loss coefficient in the absence of fading, α is the fading coefficient, and the 136 subscript *i* represents the *i*th branch. n(t) is the additive white Gaussian noise (AWGN) with single-137 sided power spectral density N_0 . We assume the path loss and fading are independent, and i.i.d 138 fading at receiver apertures because their separation (generally on the order of centimeters) is 139 sufficiently larger than coherence length (generally on the order of millimeters [34]), but not very far 140 from each other.

141 The UOT is modelled as a GG statistical distribution such that the fading coefficient α_i has the 142 probability density function (pdf) given by [14]:

$$f_{\alpha_i}(\alpha) = \frac{2\nu_i}{\left(\frac{\Omega_i}{m_i}\right)^{m_i}} \alpha^{2\nu_i m_i - 1} \exp\left(-\frac{m_i \alpha^{2\nu_i}}{\Omega_i}\right), \quad \alpha > 0$$
(3)

143 where m_i , Ω_i and v_i are the fading, scaling and shape parameters, respectively, and $\Gamma(\cdot)$ represents 144 the gamma function. The GG-distributed RV α_i is denoted as $\alpha_i \sim GG(m_i, v_i, \Omega_i)$. Other statistical 145 distributions that describe UOT such as gamma ($v_i = 0.5$) [10], Weibull ($m_i = 1$) [11], exponential 146 ($v_i = 0.5, m_i = 1$) [35] and lognormal ($m_i \rightarrow \infty, v_i \rightarrow 0$) [2] are special or limiting cases of the GG 147 distribution [13].

148 The *n*th moment of the GG-distributed fading coefficient α_i is given by:

$$\mathsf{E}[\alpha_i^n] = \left(\frac{\Omega_i}{m_i}\right)^{\frac{n}{2\nu_i}} \frac{\Gamma\left(m_i + \frac{n}{2\nu_i}\right)}{\Gamma(m_i)} \tag{4}$$

149 where $E[\cdot]$ stands for the expectation operator. Thus, the scintillation index σ_I^2 can be expressed as 150 [13]:

$$\sigma_I^2 = \frac{\mathrm{E}[\alpha_i^2] - \mathrm{E}^2[\alpha_i]}{\mathrm{E}^2[\alpha_i]} = \frac{\Gamma(m_i)\Gamma\left(m_i + \frac{1}{\nu_i}\right)}{\Gamma^2\left(m_i + \frac{1}{2\nu_i}\right)} - 1$$
(5)

To ensure that no energy loss or gain occurs during the turbulence-induced fading process, the fading coefficient is normalized (i.e., $E[\alpha_i] = 1$).

The optical intensity fluctuation due to UOT is characterized by the multiplicative fading coefficient as shown in (2), whose corresponding electrical signal-to-noise ratio (SNR) is given by [24][25]:

$$\gamma_{EGC} = \frac{(\eta I)^2 \mathbb{E}[x^2(t)] (\sum_{i=1}^N \alpha_i h_i)^2}{N_0} = \bar{\gamma} \left(\sum_{i=1}^N \alpha_i h_i' \right)^2$$
(6)

156 where

$$\bar{\gamma} = \frac{(\eta I)^2 \mathbf{E}[x^2(t)]}{N_0} \left(\sum_{i=1}^N h_i\right)^2,$$
(7)

157 and

$$h_i' = \frac{h_i}{\sum_{i=1}^N h_i'} \tag{8}$$

- 158 where $\bar{\gamma}$ denotes the average SNR per QAM symbol in DCO-OFDM without turbulence, h'_i is the
- normalized path loss. When the DC-bias is large enough to avoid any clipping distortion, the effective
- 160 SNR per received QAM symbol is given by[36]:

$$\gamma_{EGC}^{eff} = \frac{1}{1+g^2} \gamma_{EGC} = \frac{\bar{\gamma}}{1+g^2} \left(\sum_{i=1}^{N} \alpha_i h'_i \right)^2,$$
(9)

161 Assume $S = \sum_{i=1}^{N} \alpha_i h'_i = \sum_{i=1}^{N} \alpha'_i (\alpha'_i \sim GG(m_i, \nu_i, {h'_i}^{2\nu_i} \Omega_i))$ denotes the weighted sum, and then the 162 γ_{EGC}^{eff} is written as

$$\gamma_{EGC}^{eff} = \frac{\bar{\gamma}}{1+g^2} S^2. \tag{10}$$

163 **3. Performance analysis**

164 To obtain the pdf of γ_{EGC}^{eff} , the pdf of the weighted sum should be evaluated. Another GG variable 165 has been proposed to approximate the sum of multiple GG RVs. Thus, based on the pdf of the EGC 166 output SNR, analytical expressions for average BER and EC with the EGC diversity scheme over the 167 GG fading channels can be derived which are presented in forms of Fox's H-function.

168 A. The Parameters of the approximating GG RV

169 The GG-distributed weighted sum is denoted as $S \sim GG(m, v, \Omega)$, and h_i is normalized to unity for 170 simplicity. Based on the moment estimation, the parameters of *S* can be obtained by solving the 171 following nonlinear equations [31]:

$$\frac{\Gamma^2\left(m+\frac{1}{2v}\right)}{\Gamma(m)\Gamma\left(m+\frac{1}{v}\right)-\Gamma^2\left(m+\frac{1}{2v}\right)} = \frac{E^2(S)}{E(S^2)-E^2(S)'}$$
(11)

$$\frac{\Gamma^2\left(m+\frac{1}{\nu}\right)}{\Gamma(m)\Gamma\left(m+\frac{2}{\nu}\right)-\Gamma^2\left(m+\frac{1}{\nu}\right)} = \frac{E^2(S^2)}{E(S^4)-E^2(S^2)'}$$
(12)

$$\Omega = m \left(\frac{\Gamma(m) E(S)}{\Gamma\left(m + \frac{1}{2\nu}\right)} \right)^{2\nu},$$
(13)

where the *n*-th moment of *S* can be derived from the individual moments of the GG summands as[31]:

$$E(S^{n}) = \sum_{n_{1}=0}^{n} \sum_{n_{2}=0}^{n_{1}} \cdots \sum_{n_{N-1}=0}^{n_{N-2}} {n \choose n_{1}} {n_{2} \choose n_{2}} \cdots {n_{N-2} \choose n_{N-1}} E\left(\alpha_{1}^{\prime n-n_{1}}\right) E\left(\alpha_{2}^{\prime n_{1}-n_{2}}\right) \cdots E\left(\alpha_{N}^{\prime n_{N-1}}\right).$$
(14)

- 174 With the aid of MATHEMATICA or similar tools, the parameters of *S* can be calculated.
- 175 B. The average symbol error rate
- Using (9), the approximated conditional bit error probability of *L*-QAM is given by [37]:

$$p_{e} = \frac{4(\sqrt{L}-1)}{\sqrt{L}\log_{2}(L)} Q\left(S\sqrt{\frac{3\bar{\gamma}}{(L-1)(1+g^{2})}}\right) + \frac{4(\sqrt{L}-2)}{\sqrt{L}\log_{2}(L)} Q\left(3S\sqrt{\frac{3\bar{\gamma}}{(L-1)(1+g^{2})}}\right),\tag{15}$$

177 where $Q(\cdot)$ is the Gaussian *Q*-function. In the fading channels, the average BER is expressed as:

$$P_e = \int_0^\infty f_{GG}(S) p_e(S) \, dS. \tag{16}$$

178 With integration by parts and considering practical scenarios, the average BER is simplified as [38]:

$$P_e = -\int_0^\infty F_{GG}(S) \, dp_e(S), \tag{17}$$

179 where the CDF of GG distribution $F_{GG}(S)$ is given by:

$$F_{GG}(S) = \frac{\Upsilon\left(m, \frac{m}{\Omega}S^{2\nu}\right)}{\Gamma(m)},\tag{18}$$

180 and $\Upsilon(a, x)$ is the lower incomplete gamma function [39].

181 According to the definition of Gaussian Q-function, the derivative of p_e can be expressed as

$$dp_{e}(S) = -\frac{dS}{\sqrt{2\pi}} \sqrt{\frac{3\bar{\gamma}}{(L-1)(1+g^{2})}} \left\{ \frac{4(\sqrt{L}-1)}{\sqrt{L}\log_{2}(L)} \exp\left[-\frac{3\bar{\gamma}S^{2}}{2(L-1)(1+g^{2})}\right] + \frac{12(\sqrt{L}-2)}{\sqrt{L}\log_{2}(L)} \exp\left[-\frac{27\bar{\gamma}S^{2}}{2(L-1)(1+g^{2})}\right] \right\}.$$
(19)

Substituting (18) and (19) to (17) and then using variable substitution and the Gauss-LaguerreQuadrature shown as [40]:

$$\int_{0}^{\infty} x^{-1/2} e^{-x} f(x) dx \cong \sum_{i=1}^{n} H_{i} f(x_{i})$$
(20)

184 equation (17) can be approximated by:

$$P_{e} = \frac{1}{2\sqrt{\pi}\Gamma(m)} \sum_{i=1}^{n} H_{i} \left[\frac{4(\sqrt{L}-1)}{\sqrt{L}\log_{2}(L)} \Upsilon\left(m, \frac{m}{\Omega} \left(\sqrt{\frac{2x_{i}(L-1)(1+g^{2})}{3\bar{\gamma}}}\right)^{2\nu}\right) + \frac{4(\sqrt{L}-2)}{\sqrt{L}\log_{2}(L)} \Upsilon\left(m, \frac{m}{\Omega} \left(\sqrt{\frac{2x_{i}(L-1)(1+g^{2})}{27\bar{\gamma}}}\right)^{2\nu}\right) \right],$$

$$(21)$$

185 where x_i is the *i*th zero of the Laguerre polynomial $L_n^{-1/2}(x)$ and H_i is the corresponding weight 186 coefficient detailed in [40].

187 C. Ergodic capacity

188 Using (10), the EC of the EGC diversity systems over fading channels in bps/Hz is given by:

$$\bar{C} = \frac{\mathrm{E}\left[\ln(1+\gamma_{EGC}^{eff})\right]}{\ln 2} = \frac{1}{\ln 2} \mathrm{E}\left[\ln\left(1+\frac{\bar{\gamma}}{1+g^2}S^2\right)\right].$$
(22)

189 Let $Z = S^2$, and thus Z satisfies $Z \sim GG(m, v/2, \Omega)$. Then, (22) can be expressed as

$$\bar{C} = \frac{1}{\ln 2} \int_0^\infty \ln\left[1 + \frac{\bar{\gamma}}{1+g^2} Z\right] \frac{v}{\Gamma(m)} \left(\frac{\Omega}{m}\right)^{-m} Z^{m\nu-1} \exp\left(-\frac{m}{\Omega} Z^\nu\right) dZ.$$
(23)

190 By substituting $Y = \left(\frac{m}{\alpha}\right)^{1/\nu} Z$ in (23), we have:

7 of 14

$$\bar{C} = \frac{1}{\ln 2} \int_0^\infty \ln\left[1 + \frac{\bar{\gamma}}{1+g^2} \left(\frac{m}{\Omega}\right)^{-1/\nu} Y\right] \frac{\nu}{\Gamma(m)} Y^{m\nu-1} \exp(-Y^\nu) \, dY.$$
(24)

To simplify (24) in the form of Fox's H function, firstly we express the logarithmic function in theforms of Meijer's G function given by [41]:

$$\ln(1+x) = G_{2,2}^{1,2} \left[x \, \Big| \, \substack{1,1 \\ 1,0} \right]. \tag{25}$$

193 Furthermore, using the transforms between Meijer's G function and Fox's H function given by [42]:

$$H_{p,q}^{e,f}\left[x \begin{vmatrix} (a_i, 1)_{1,p} \\ (b_i, 1)_{1,q} \end{vmatrix}\right] = G_{p,q}^{e,f}\left[x \begin{vmatrix} (a_i)_{1,p} \\ (b_i)_{1,q} \end{vmatrix}\right],$$
(26)

and then using the product of power and exponential functions expressed by [42]:

$$H_{0,1}^{1,0}\left[x\left|\frac{1}{(b,\beta)}\right] = \frac{1}{\beta}x^{b/\beta}\exp(-x^{\frac{1}{\beta}}),$$
(27)

195 equation (24) is written as:

$$\bar{C} = \frac{1}{\ln 2\Gamma(m)} \int_0^\infty Y^{m\nu-\nu-1} H_{0,1}^{1,0} \left[\frac{\bar{\gamma}}{1+g^2} \left(\frac{m}{a} \right)^{-1/\nu} Y \left| \begin{pmatrix} 1,1 \end{pmatrix}, \begin{pmatrix} 1,1 \end{pmatrix} \right| H_{0,1}^{1,0} \left[Y \left| \frac{1}{(1,1/\nu)} \right] \right] dY.$$
(28)

196 Finally, using integral formulas involving the H-function given by [42,2.8.4], we have:

$$\bar{C} = \frac{1}{\ln 2 \Gamma(m)} H_{3,2}^{1,3} \left[\frac{\bar{\gamma}}{1+g^2} \left(\frac{m}{\Omega} \right)^{-1/\nu} \Big|_{(1,1),(1,1),(1-m,1/\nu)}^{(1,1),(1-m,1/\nu)} \right].$$
(29)

197 By using (29), we can evaluate the EC of the EGC diversity systems over GG fading channels.

198 4. Results and Discussion

199 In this section, numerical results for the average BER and EC based on the analytical expressions 200 and MATHEMATICA are presented for different diversity orders under various GG fading 201 conditions. To verify the analytical results, the results of the MC simulations, using MATLAB, are 202 also presented. Based on the study in [13], two fading channel scenarios are considered and their 203 corresponding parameters of GG RVs are shown in Table I.

204

Table I the parameters of i.i.d GG-distributed fading channels based on Table III and IV of [13]

Channel condition	<i>m</i> _i	V _i	Ω_i	σ_I^2
Salinity random variations	1.62	0.72	1.1	0.31
Temperature random variations mixed presence of air bubbles	1.4	0.42	0.94	1.02

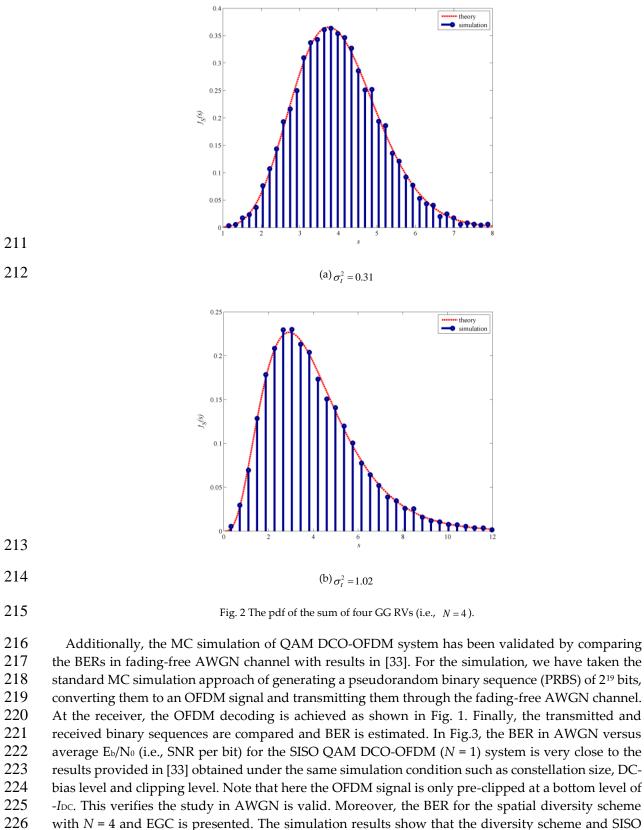
Fig.2 depicts the pdf of the sum of four i.i.d GG-distributed RVs, i.e., for a diversity order of 4. The theoretical pdf is evaluated using (10) to (13), which is verified by Monte Carlo simulation. Four i.i.d

206 theoretical pdf is evaluated using (10) to (13), which is verified by Monte Carlo simulation. Four i.i.d 207 GG-distributed RVs are generated based on the inverse transform method. Then, the histogram of

208 their sum is obtained to compare with the theoretical pdf. Fig.2 clearly shows a good agreement

between the theoretical and simulation results for $\sigma_l^2 = 0.31$ and 1.02, which is the basis for average

210 BER and EC evaluation in the following section.



scheme have the same BER in AWGN, i.e., no diversity gain was observed in the absence of turbulence-induced fading. Hence, the SNR gain in the turbulence channel is attributed to the

diversity scheme used.



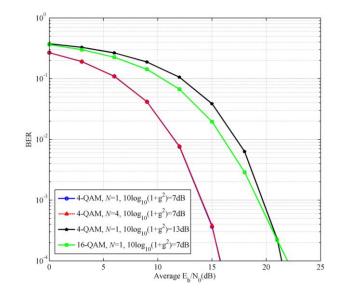
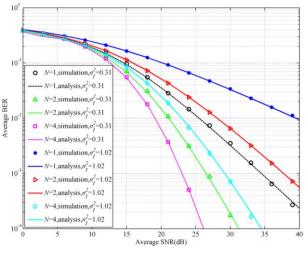






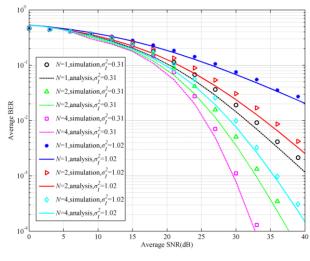
Fig.3 BERs versus average Eb/No for 4 & 16-QAM DCO-OFDM scheme in AWGN based on MC simulation

232 Next, we analyzed and compared the BER performance of the diversity scheme with EGC over 233 GG-distributed fading channels. The UOWC channel is slow fading and hence, a constant fading 234 coefficient is considered over an OFDM symbol which changes with OFDM symbols [13]. The 235 analytical and simulated average BERs versus average SNR per QAM symbol for the 4&16-QAM-236 OFDM scheme over GG fading channels with $\sigma_1^2 = 0.31$ and 1.02 are shown in Fig. 4, where the 237 normalized bias is assumed as g = 3 to ensure no clipping distortion. It is observed that there is a 238 close match between the analytical and simulated results in weak and strong turbulence channels, 239 thereby validating the accuracy of approximated analytical expressions. The agreement between 240 analytical and simulated BERs in the case of 4-QAM is better than that in the case of 16-QAM because 241 the truncation error in (15) increases with increasing constellation size.



242 243

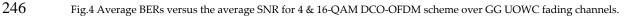
(a) 4-QAM



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(b) 16-QAM

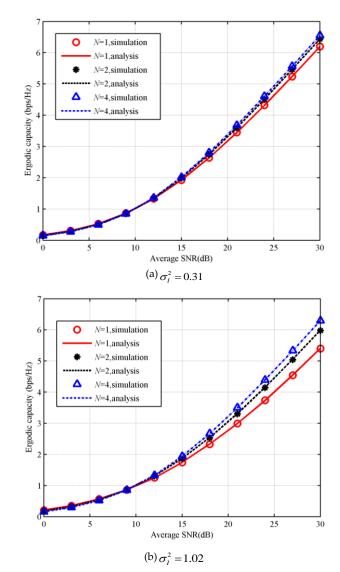
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247 Furthermore, in Fig. 4 it is clearly shown that the BER performance degrades with the increasing 248 scintillation index, and spatial diversity can effectively mitigate the effect of turbulence. A large 249 diversity gain can be obtained by increasing the diversity order. For example, seen from Fig.4(a), for 250 a weak turbulence channel with $\sigma_t^2 = 0.31$, the diversity order of 2 requires ~3.5 dB higher SNR than 251 that for diversity order of 4 to achieve a BER of 10⁻³. For a strong turbulence channel with $\sigma_1^2 = 1.02$, 252 the diversity gain difference increases to 8.5 dB. This clearly demonstrates the advantage of a large 253 diversity order for strong turbulence channels. By comparing Fig.4(a) and (b), the trade-off between 254 spectral efficiency and reliability is shown as that 16-QAM system requires higher SNR or larger 255 diversity order than 4-QAM to achieve the same BER performance.

256 Fig.5 illustrates the analytical and simulated EC per unit bandwidth for no diversity and diversity 257 orders of 2 and 4 over GG-distributed fading channel. In the simulation, 10⁵ GG random samples are 258 generated for each branch to evaluate the EC for receiver diversity with EGC. Fig.5 demonstrates that 259 there is a good agreement between the simulation and analytical results, validating the analytical 260 expression. Similar to BER, by comparing Fig.5(a) and (b), ECs decrease as the turbulence strength 261 increases. Unlike the case of BER performance, the improvement in EC due to the diversity scheme 262 is not obvious in a weak turbulence channel. The diversity gain of N = 2 and 4 is close, as the diversity 263 gain saturates at a higher diversity order. However, with increasing the turbulence strength, spatial 264 diversity is necessary to ensure a large EC, which can be seen from Fig.5. With the scintillation index 265 changing from 0.31 to 1.02, ECs drop 0.8, 0.4 and 0.2 bps/Hz for the scheme of N=1, 2 and 4 at SNR = 266 30 dB, respectively, demonstrating the necessity of spatial diversity. Thus, the results are useful to 267 practical system design in terms of the relation among average BER, EC, diversity order and SNR

268 over various GG fading channels.





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Fig.5 ECs versus average SNR in GG fading channels.

274 5. Conclusion

275 In this paper, the spatial diversity with EGC was proposed to combat turbulence-induced fading 276 impairments in UWOC systems over GG channels. Based on the approximation of the sum of GG 277 RVs, the average BER and EC for QAM-DCO-OFDM were evaluated. Using Gauss-Laguerre 278 quadrature integral, a closed-form expression of the average BER is derived. In addition, with the 279 help of transforms and integral formulas involving Fox's H function, the EC is given in the forms of 280 Fox's H function. Based on the derived closed-form expressions, the analytical results of BERs for 4 281 & 16-QAM DCO-OFDM with diversity schemes over GG fading channels are calculated and 282 compared with the Monte-Carlo simulation results. In addition, the analytical and simulated ECs per 283 unit bandwidth are also presented. All the results showed excellent agreement between the analysis 284 and simulation, validating the theoretical analysis. It is shown that increasing diversity order 285 improves BER performance and EC, especially in strong turbulence. However, the gain saturates at 286 higher diversity order. Meanwhile, cost and complexity increase with increasing diversity order. 287 Hence, a careful trade-off is required to optimize the performance with a cost-effective solution. The 288 obtained results are useful for designing, predicting and evaluating the DCO-OFDM spatial diversity 289 UOWC system in various fading scenarios.

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